

Objectives for our Discussion of Separations

Basics

1. Define, understand, and use key terms such as retention time, retention factor, selectivity, and resolution.
2. Predict changes in separation metrics upon a change in conditions (e.g., column length, particle size, flow rate, etc.).

Retention

1. (GC/LC) Predict the effect of a change in conditions on relative retention (e.g., change in stationary phase, mobile phase, flow rate, etc.).
2. (GC/LC) Use chemical and physical reasoning to explain the basis of retention, given a specific scenario (e.g., why is benzyl alcohol less retained than benzene in RPLC?).

Peak Broadening

1. (GC/LC) Predict the effect of a change in conditions (e.g., mobile phase type, temperature, particle size, etc.) on peak properties (e.g., height, width, retention time).
2. (GC/LC) Use chemical and physical reasoning to explain the basis of peak broadening, given a specific scenario (e.g., why is the peak for anthracene broader than the peak for benzene under RPLC conditions?).

GC Retention

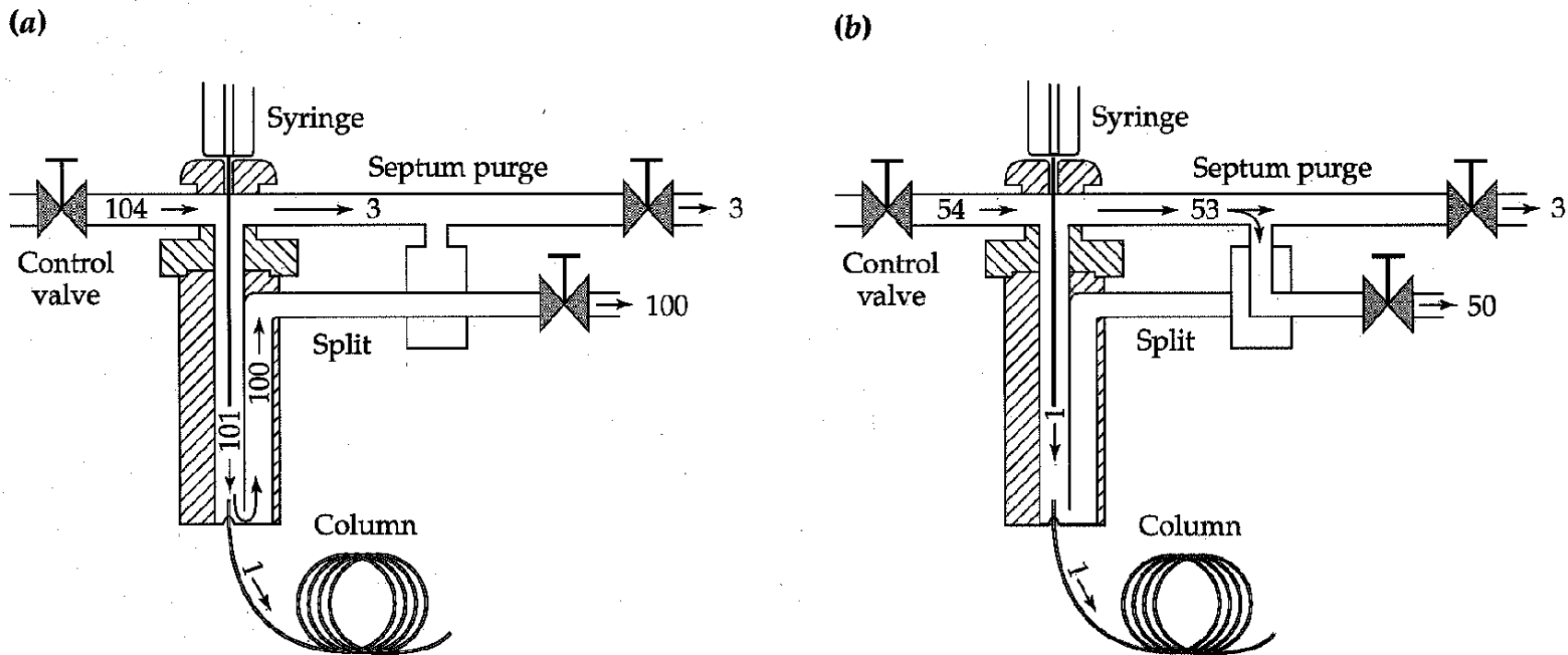


FIGURE 15.3 ▲

Schematic illustration of the structure and operation of a sample splitter.

(Left) Split configuration. The apparatus is enclosed in an oven at a temperature higher than that of the capillary column. The sample is injected, vaporized, and carried toward the top of the column by the carrier gas. The needle valve allows a precise adjustment of the fraction of sample that enters the column while the larger part is driven out through an exhaust.

(Right) Splitless configuration. With the valve closed, the injector acts as a typical injector for a packed column, in which all of the sample flows to the column. The splitter shown also includes a **septum purge** valve to eliminate volatiles that arise from septum outgassing and decomposition. [Redrawn from HP 5890 Tutorial, courtesy of Hewlett-Packard]

TABLE 27-3 Some Common Liquid Stationary Phases for GLC

| Stationary Phase | Common Trade Name | Maximum Temperature, °C | Common Applications |
|-------------------------------------------|--------------------------|--------------------------------|-------------------------------------------------------------------------------------|
| Polydimethyl siloxane | OV-1, SE-30 | 350 | General-purpose nonpolar phase, hydrocarbons, polynuclear aromatics, steroids, PCBs |
| 5% Phenyl-polydimethyl siloxane | OV-3, SE-52 | 350 | Fatty acid methyl esters, alkaloids, drugs, halogenated compounds |
| 50% Phenyl-polydimethyl siloxane | OV-17 | 250 | Drugs, steroids, pesticides, glycols |
| 50% Trifluoropropyl-polydimethyl siloxane | OV-210 | 200 | Chlorinated aromatics, nitroaromatics, alkyl substituted benzenes |
| Polyethylene glycol | Carbowax 20M | 250 | Free acids, alcohols, ethers, essential oils, glycols |
| 50% Cyanopropyl-polydimethyl siloxane | OV-275 | 240 | Polyunsaturated fatty acids, rosin acids, free acids, alcohols |

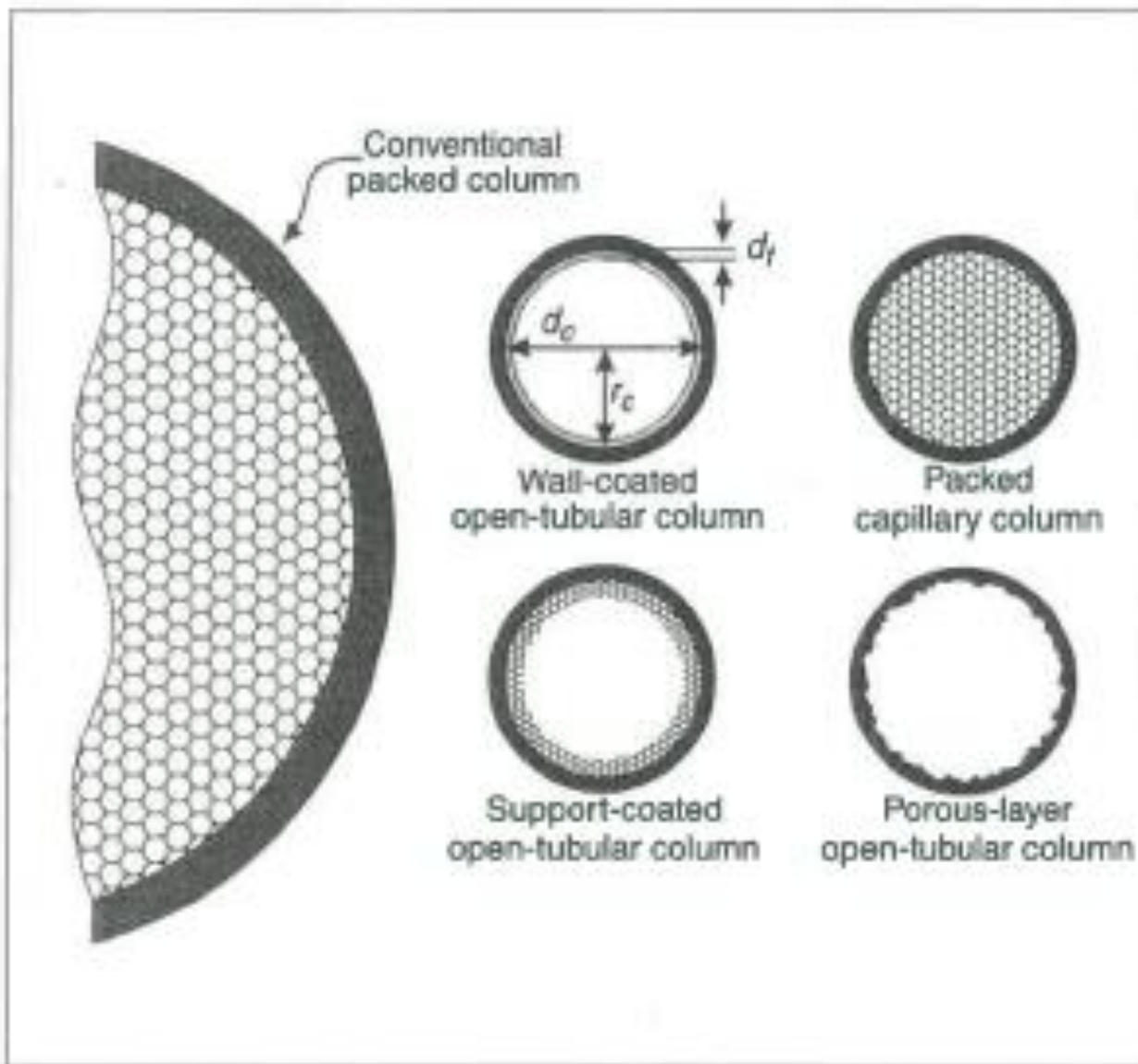


Figure 25. Types of open-tubular GC columns compared to a packed column. Drawn to scale for 0.53-mm i.d. open-tubular and 2-mm i.d. packed columns.

| Column Type | Open Tube | | Open Tube | | Open Tube/Packed Bed | |
|-----------------------|-----------------------------------------|-----|-----------------------------|-----|--------------------------------------|-----|
| Column Diameter | Narrow ~ 0.1-0.3 mm | | Narrow ~ 0.25-0.32 mm | | Wide > 0.5 mm | |
| S.P. Film Thickness | Thin ~ 0.2 microns | | Thick ~ 1-2 microns | | Thick - 2-5 microns (open tube only) | |
| | | Why | | Why | | Why |
| Efficiency | Best | | Good | | Poor | |
| Separation speed | Fast | | Moderate | | Slow | |
| Analyte Capacity | Poor | | Good | | Best | |
| | | | | | | |
| Preferred Application | High speed, high resolution separations | | Low boiling point compounds | | Anybody can do it | |
| | High boiling point compounds | | Trace analysis | | Low boiling point compounds | |
| | Thermally unstable compounds | | | | | |

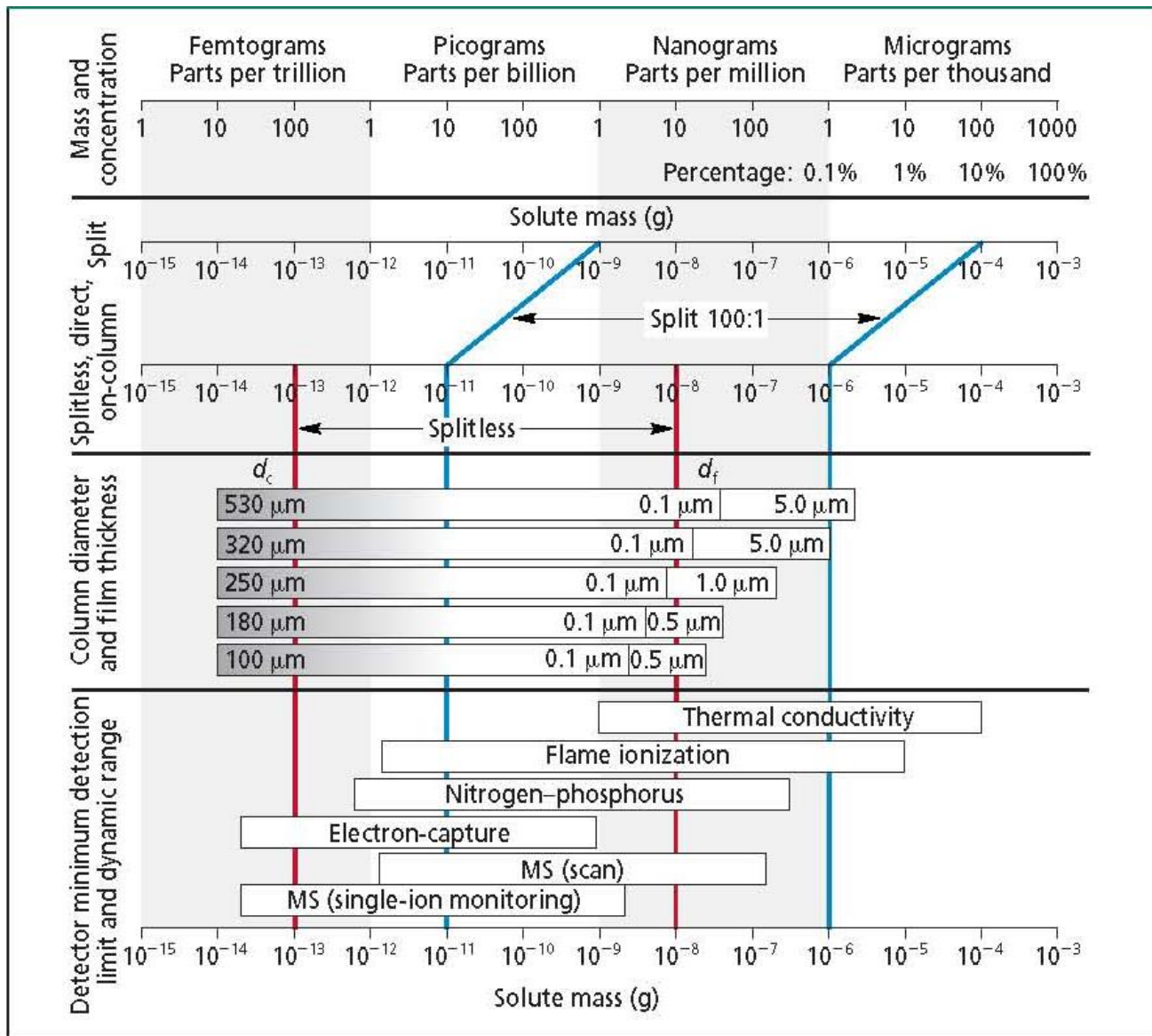


Figure 1: GC dynamic range nomogram. Concentrations are expressed in grams per microliter. Column data are from references 2 and 3 and manufacturers' information. Detector data are from reference 4 and manufacturers' aggregated 1999 specifications. Individual detector models will vary — always obtain exact specifications from the manufacturer.

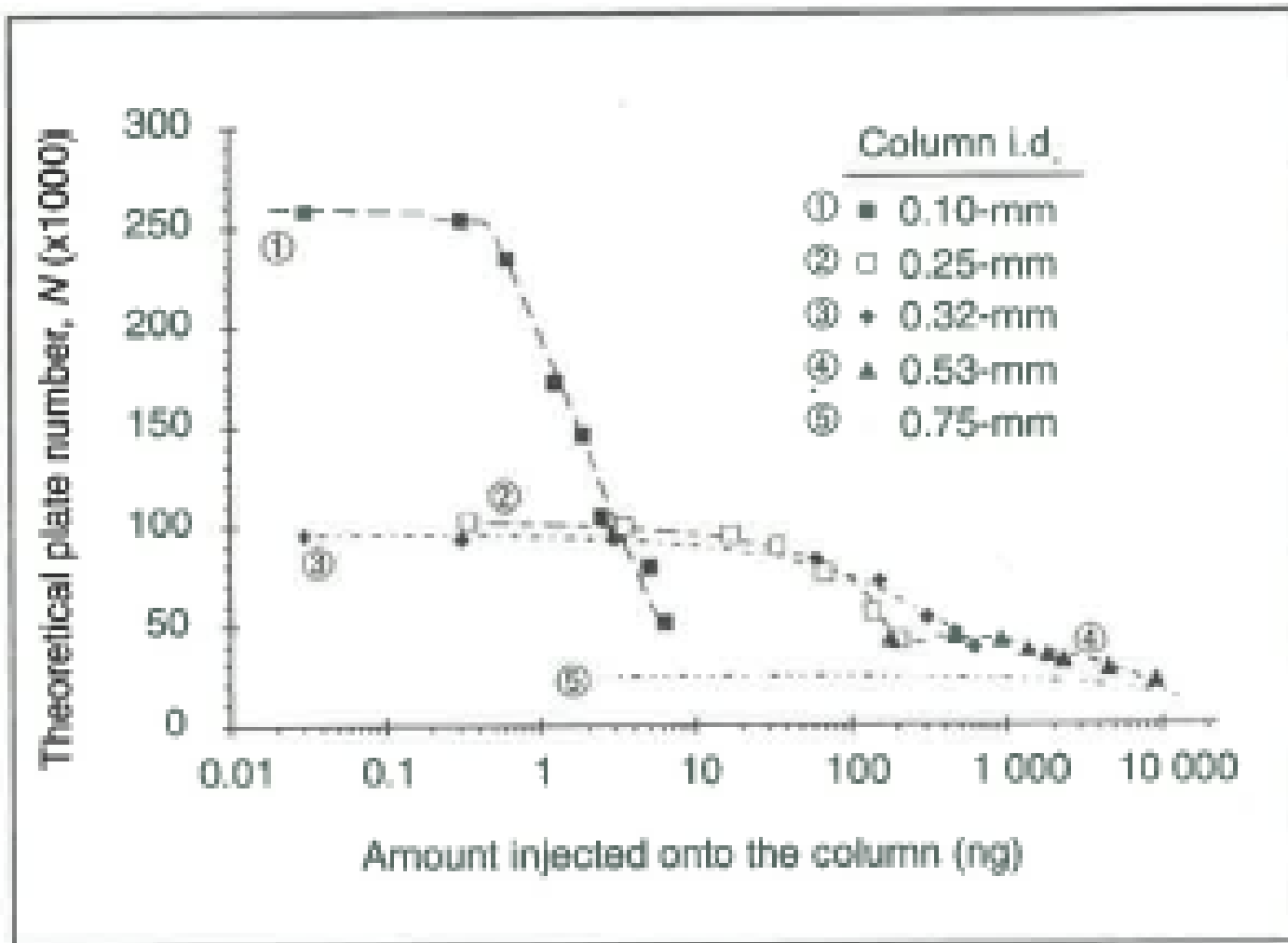


Figure 32. Number of theoretical plates calculated for *n*-undecane as a function of the injected sample amount. The column i.d. is indicated in the figure. All data refers to 25-m column lengths. See Table 13 on page 100 for the analytical conditions^[75].

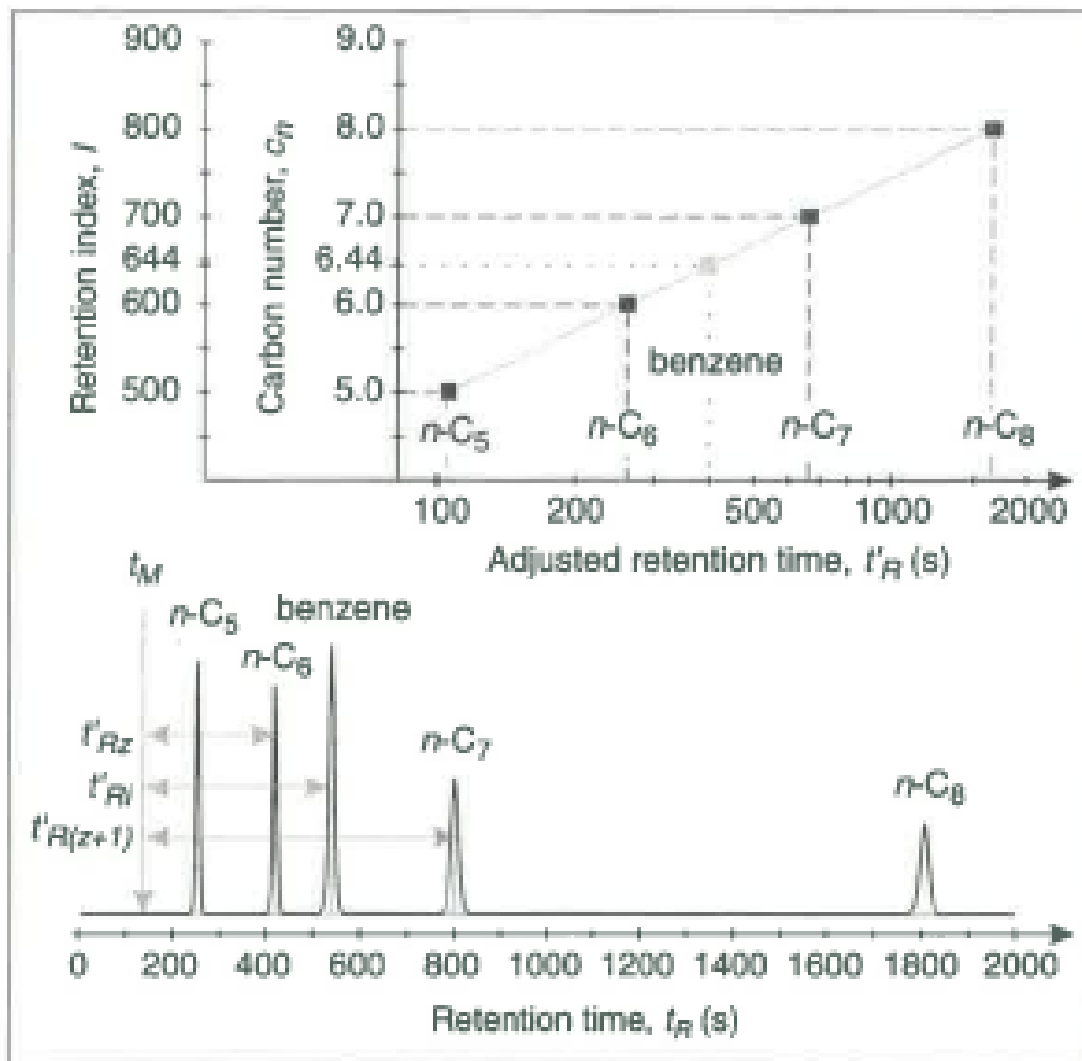


Figure 10. Calculation of the isothermal retention index. Solute i is benzene; its retention index is calculated as 644. Data refer to a 0.25-mm i.d. open-tubular column coated with methylsilicone phase and operated at 60 °C. See Table 6 on the next page for numerical data.

$$I = 100 \left(z + \frac{\log t'_{Ri} - \log t'_{Rz}}{\log t'_{R(z+1)} - \log t'_{Rz}} \right)$$

| Peak | t_R (s) | t'_R (s) | I |
|----------------------|-----------|------------|-----|
| t_M | 147.9 | — | — |
| $n\text{-C}_5$ | 251.8 | 103.9 | 500 |
| $n\text{-C}_6$ (z) | 410.0 | 262.1 | 600 |
| <i>benzene</i> (i) | 543.3 | 395.4 | 644 |
| $n\text{-C}_7$ (z+1) | 809.2 | 661.3 | 700 |
| $n\text{-C}_8$ | 1816.8 | 1668.9 | 800 |

Table 6. Data for Figure 10.

Example: Calculating the retention index. Table 6 lists the data from Figure 10. Taking the adjusted retention times (t'_R) for $n\text{-C}_6$, $n\text{-C}_7$, and the analyte (*i*), we can calculate the retention index, I :

$$I = 100 \times \left(6 + \frac{\log (395.4) - \log (262.1)}{\log (661.3) - \log (262.1)} \right) = 644$$

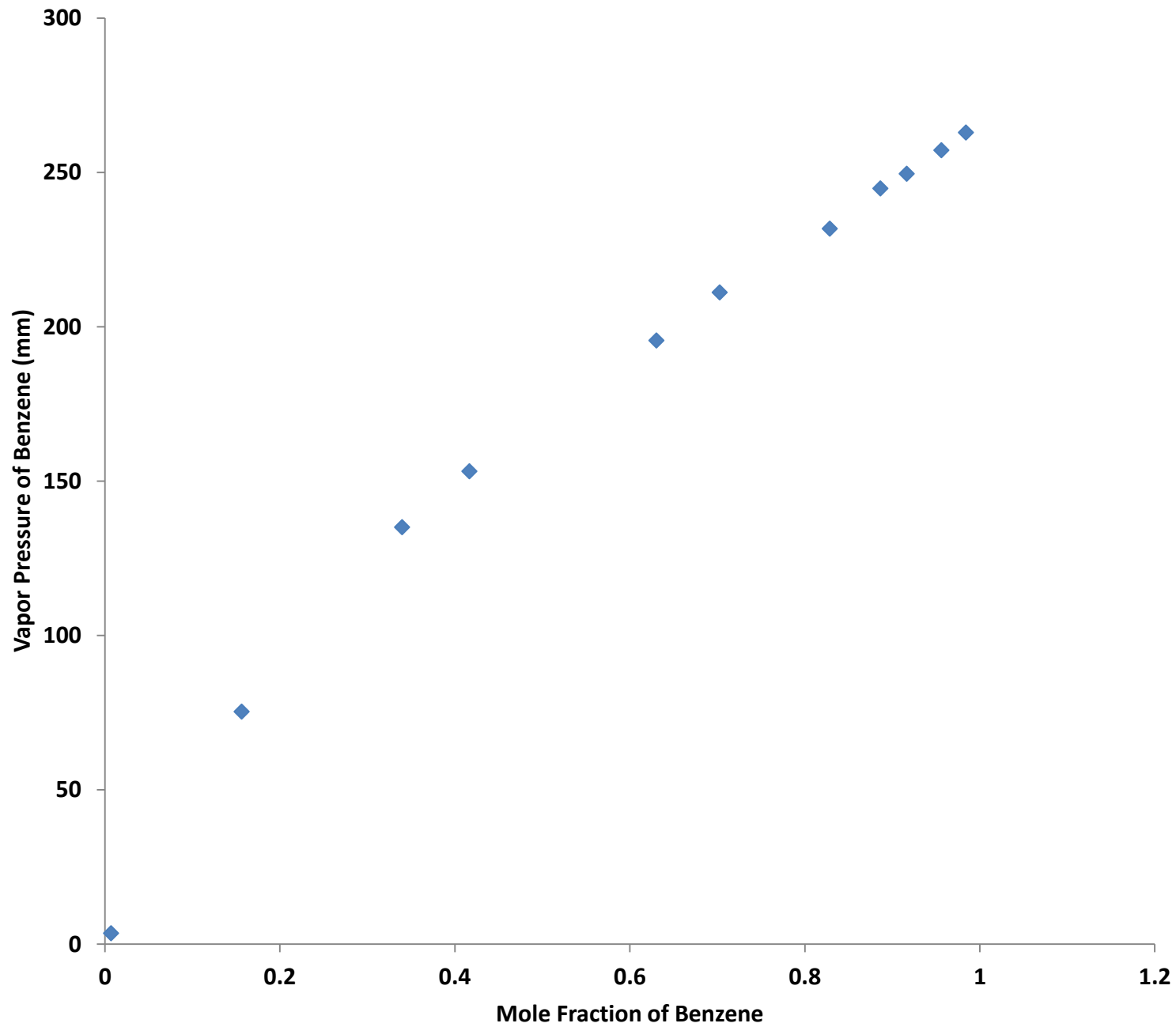


TABLE 3.17

TYPICAL FIGURES TO TEST THE VALIDITY OF THE ADDITIVITY OF GROUP RETENTION INDICES

| | | (a) Sample retention indices ^a | | |
|-----|--------------------------------|-------------------------------------------|-----------------------|-----------------------|
| No. | Solute | Retention index | | |
| | | <i>I</i> ^b | <i>I</i> ^c | <i>I</i> ^d |
| 1 | 1-Pentene | 483 | 402 | 553 |
| 2 | <i>n</i> -Propanol | 513 | 662 | 1132 |
| 3 | Allyl alcohol | 504 | 672 | 1203 |
| 4 | Propyl acetate | 653 | 737 | 1032 |
| 5 | Allyl acetate | 638 | 737 | 1085 |
| 6 | Butyl methyl ether | 594 | 640 | 782 |
| 7 | Ethylene glycol dimethyl ether | 607 | 683 | 999 |
| 8 | <i>n</i> -Butanol | 620 | 759 | 1243 |
| 9 | 1,4-Butane diol | 900 | 1170 | 2100 |
| 10 | <i>iso</i> -Pentane | 475 | 475 | 475 |
| 11 | 2-Butanone | 552 | 648 | 891 |
| 12 | 3-Methyl-2-butanone | 619 | 708 | 1008 |
| 13 | Methylal | 476 | 545 | 788 |
| 14 | Methoxymethylal | 654 | 745 | 1094 |
| 15 | Dimethoxymethylal | 826 | 937 | 1372 |

LC Retention in Three Parts

LC Retention – Part I

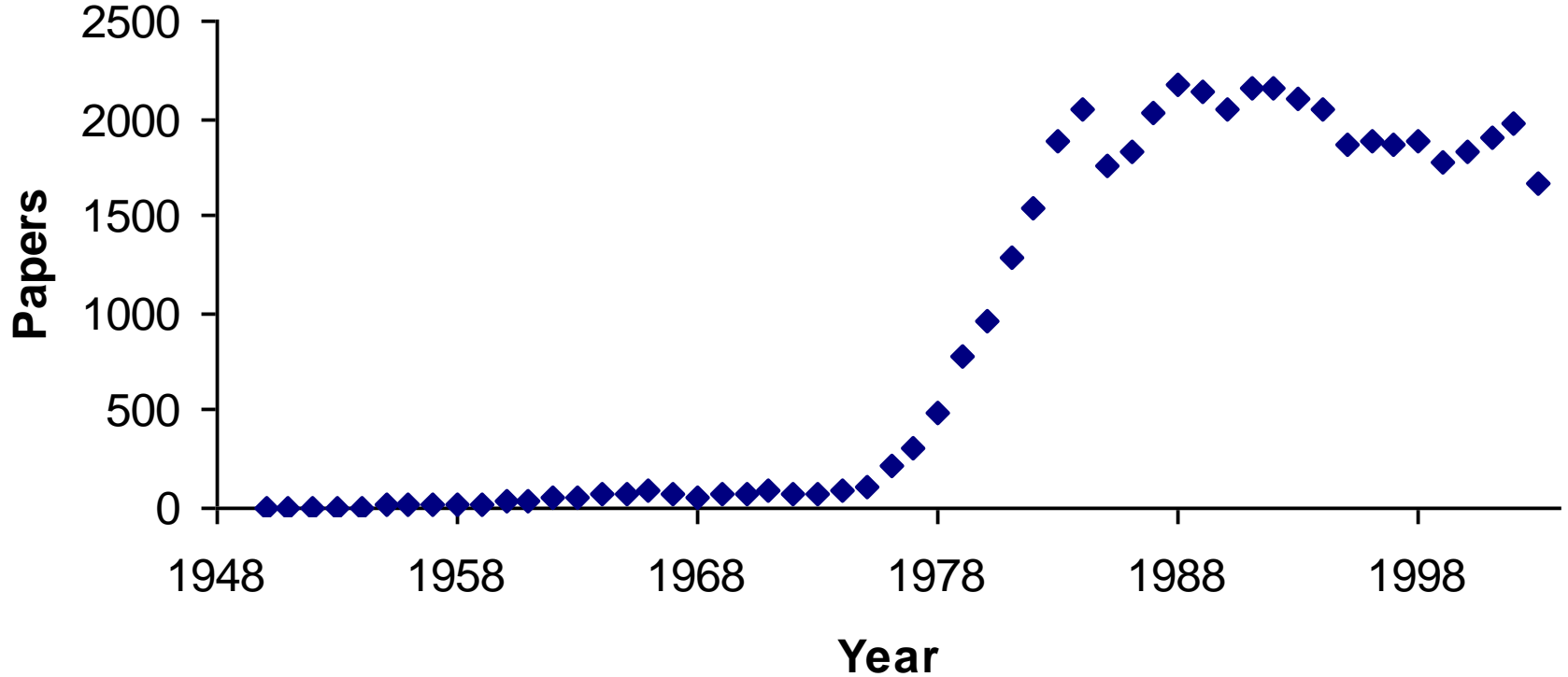
Context for and Empirical Knowledge of RPLC

Complementarity of GC and LC

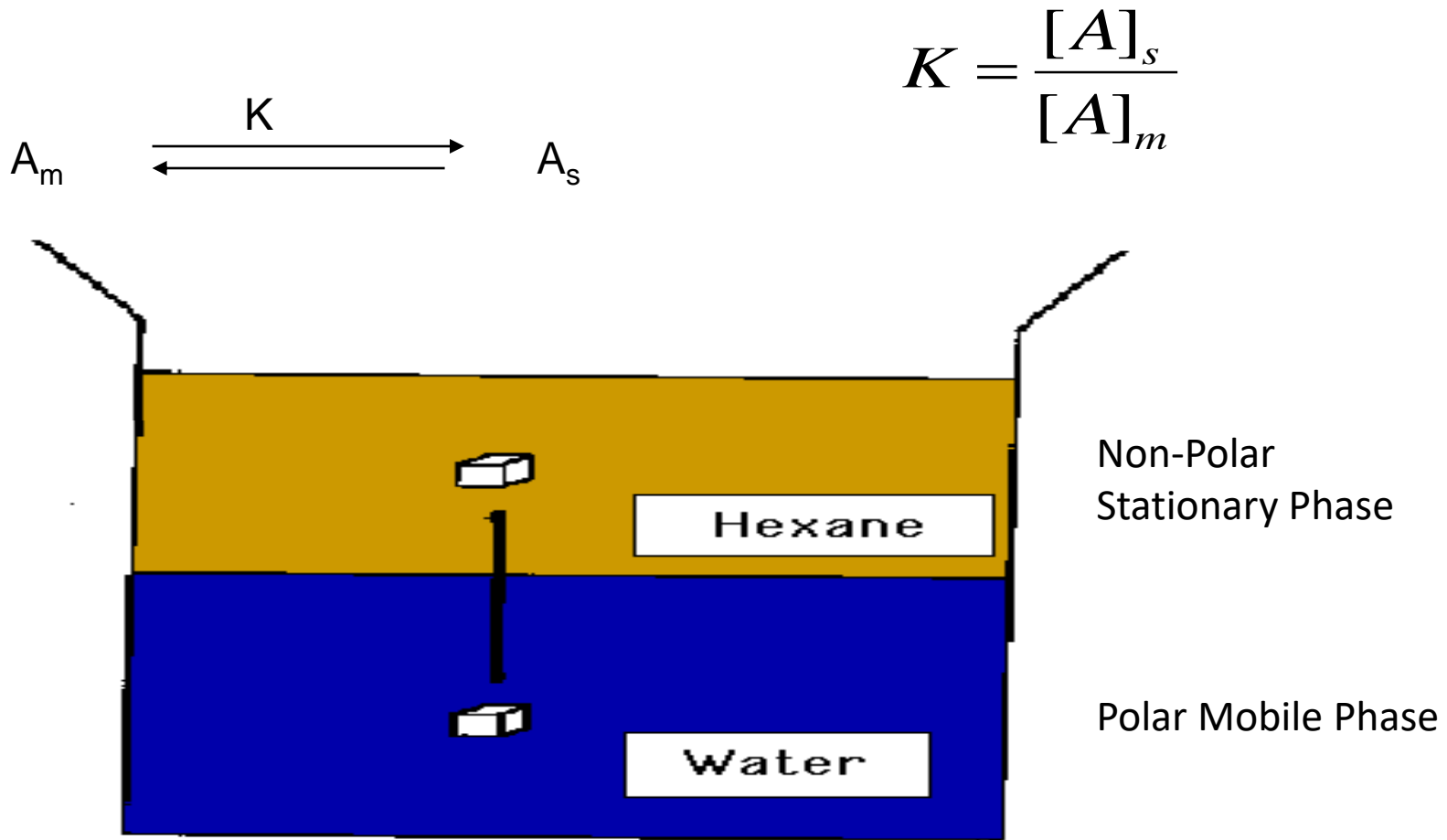
Column types (physical) and phases (chemistries)

History of RPLC

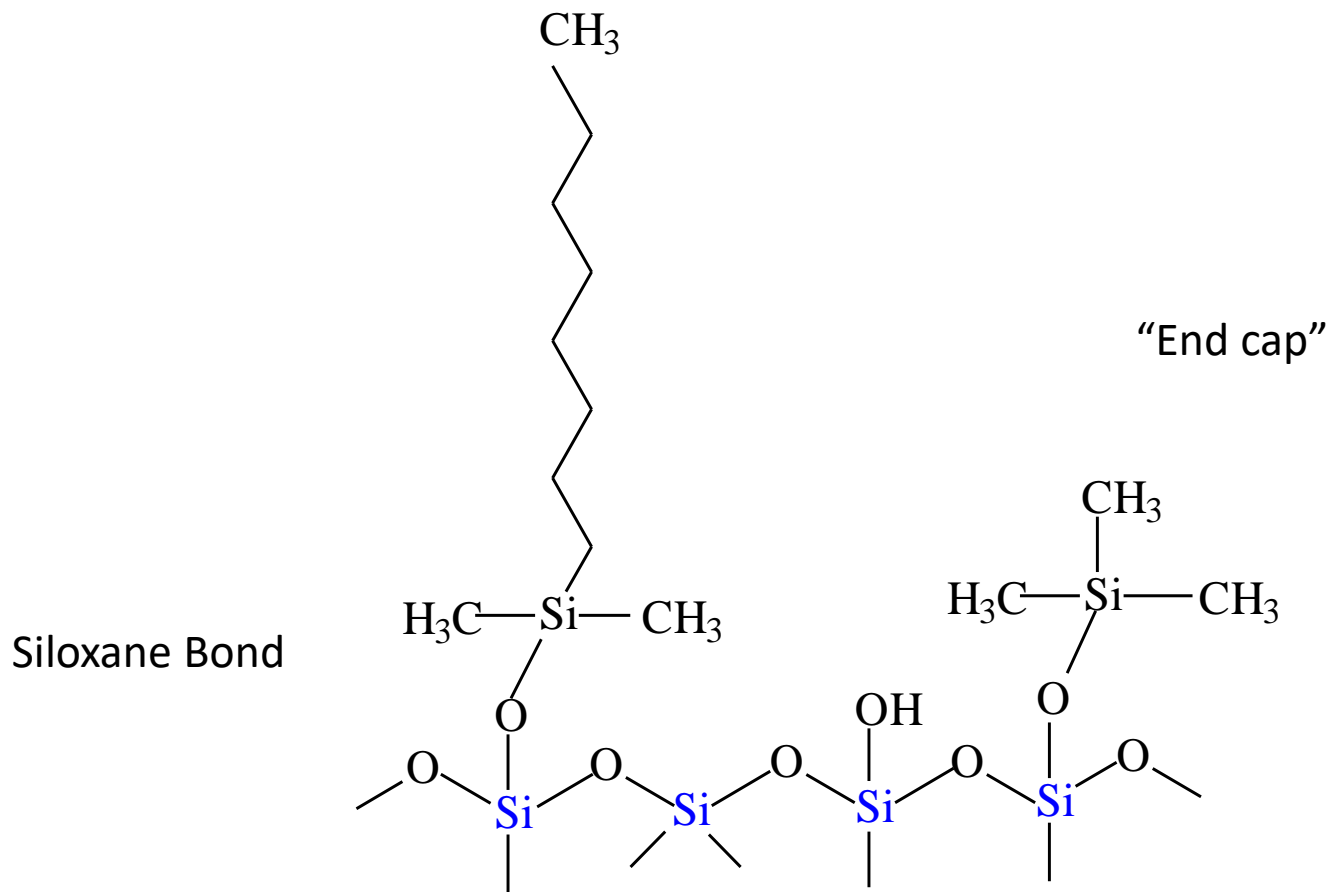
RPLC Papers/Year



Partition Model of RPLC



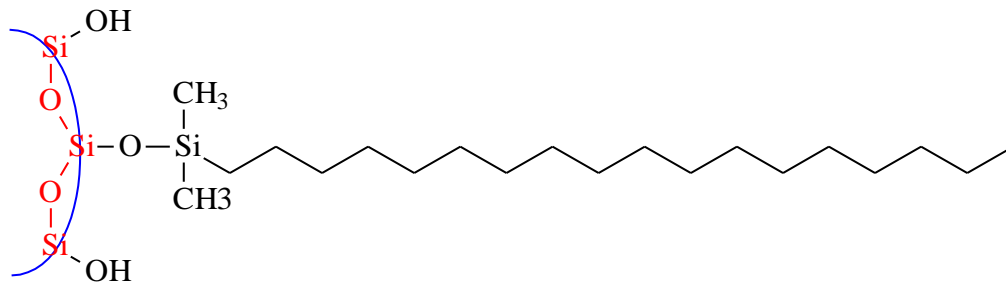
Conventional Bonded Phases



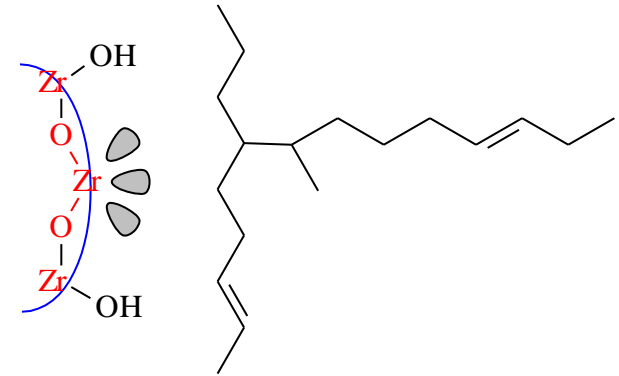
Endcapped octylsilane bonded phase

Typical silanes are C₈ and C₁₈ (octadecylsilane = ODS)

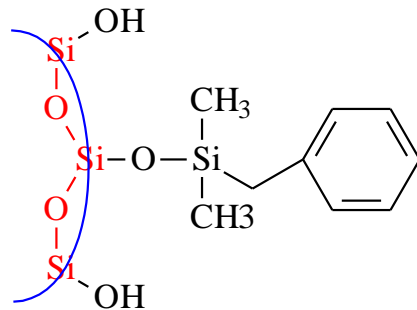
Structures of Stationary Phases



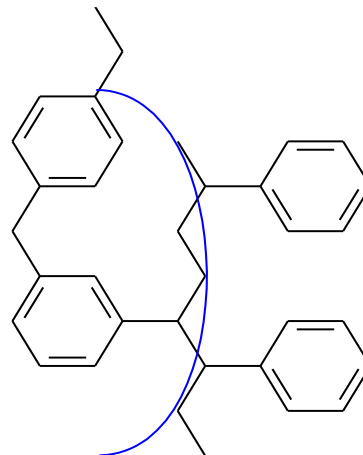
C18-SiO₂



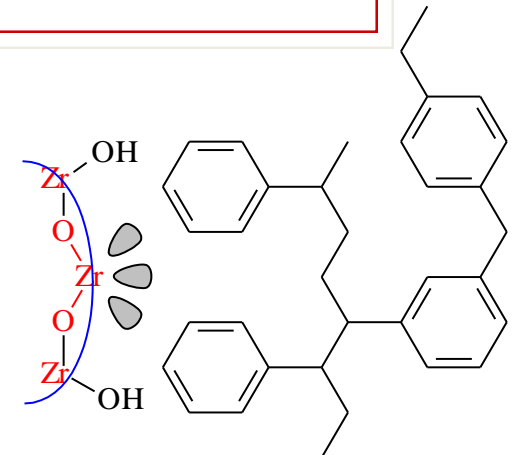
PBD-ZrO₂
PBD=Polybutadiene



Phenyl-SiO₂

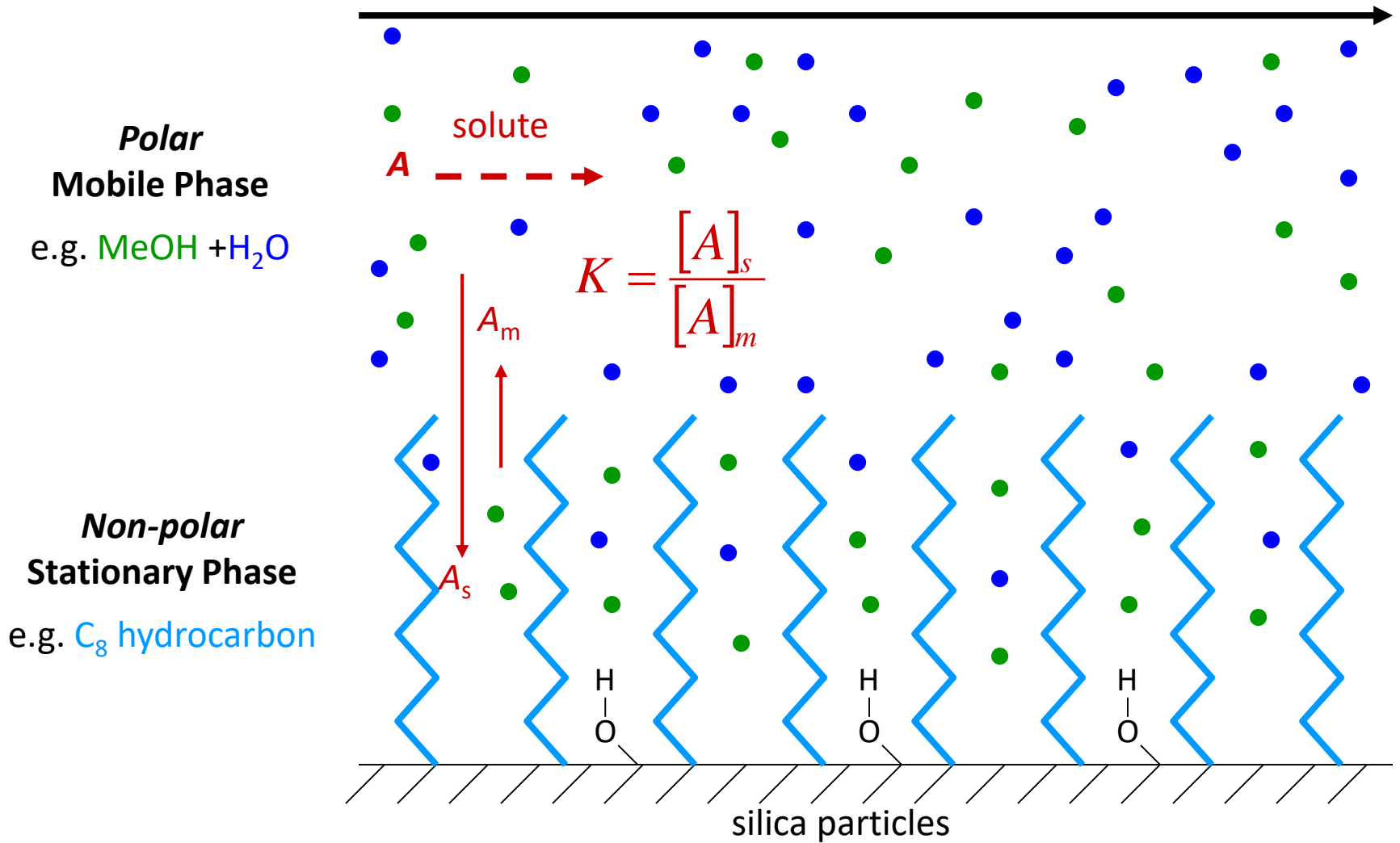


PRP-1
PRP=Polystyrene-Divinylbenzene

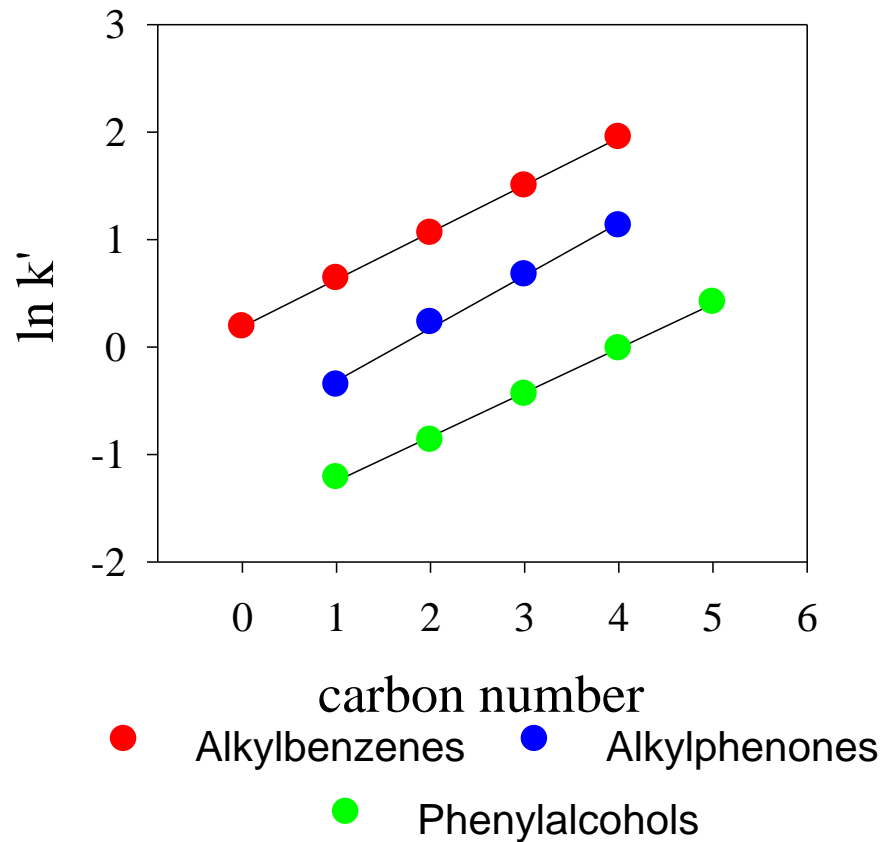


PS-ZrO₂
PS=Polystyrene

RPLC Retention



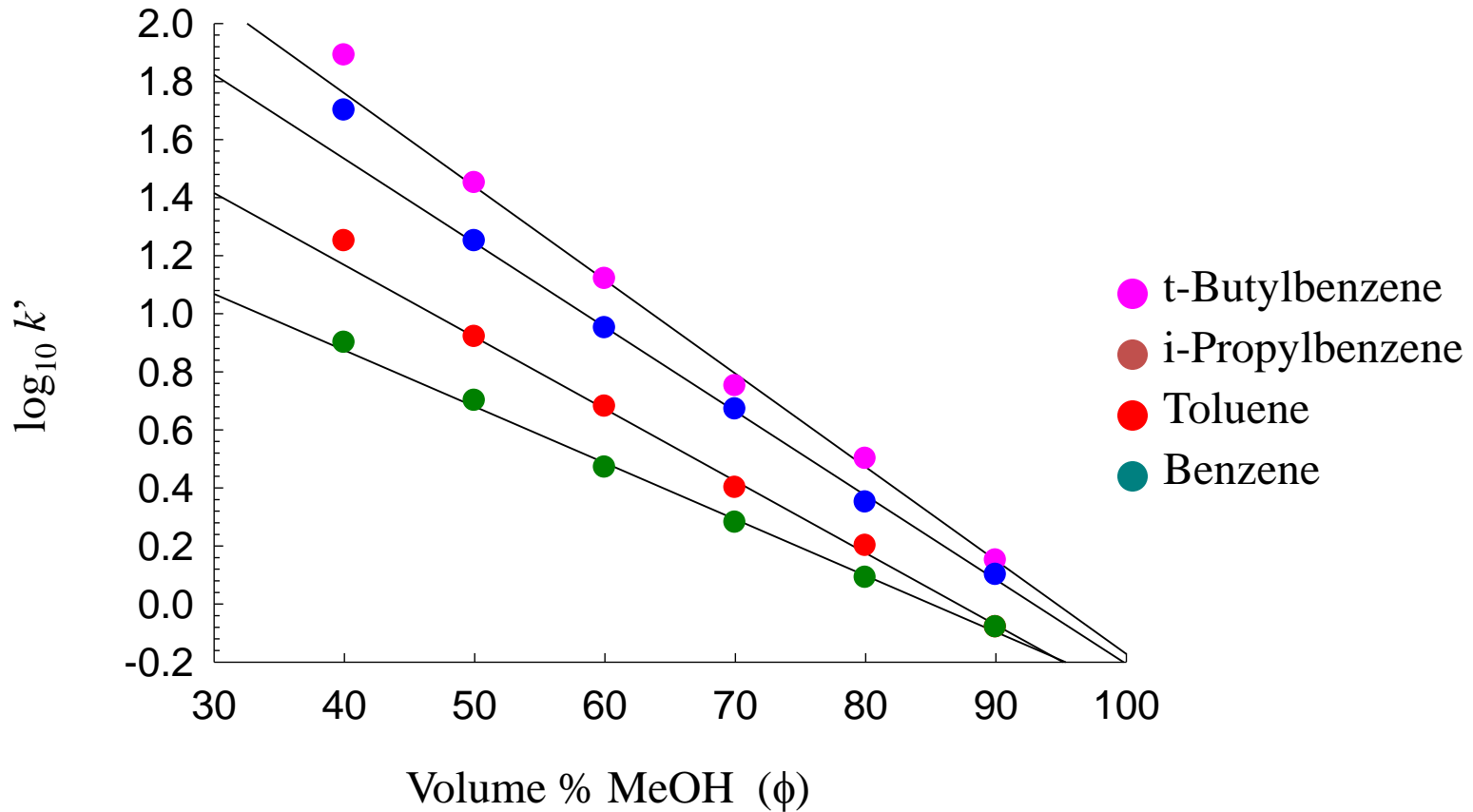
Reversed Phase Characteristics



$$\ln k' = A + Bn_{CH_2}$$

Martin Eqn.

Effect of Mobile Phase Modifier in RPLC

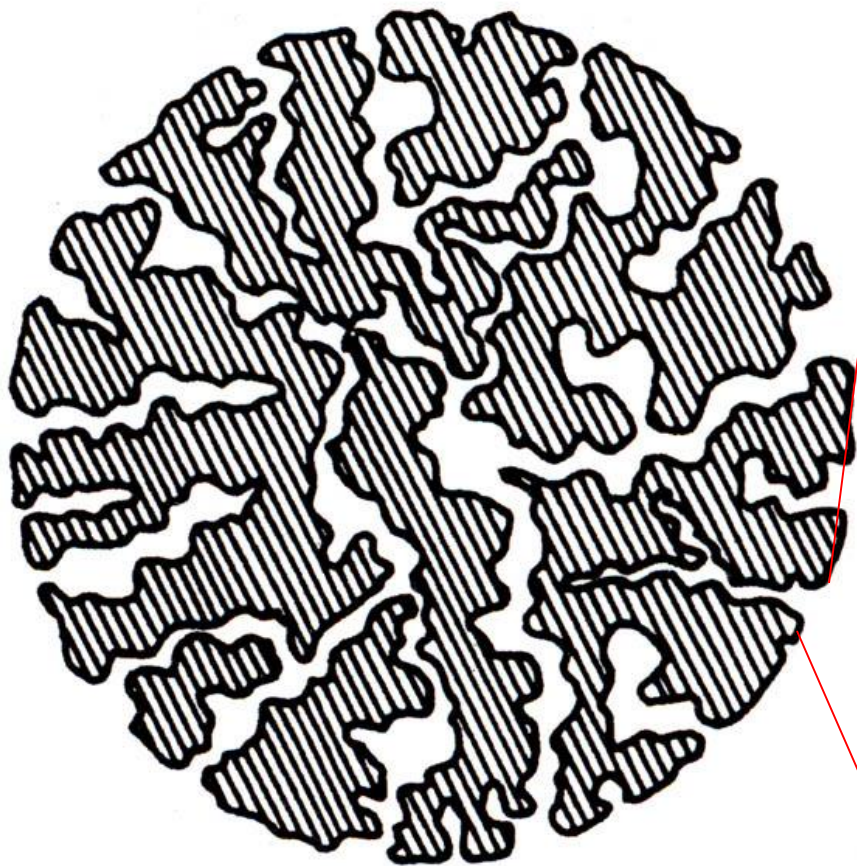


$$\log k' = \log k'_{\text{w}} - S * \phi; \text{LSST (Snyder Eqn.)}$$

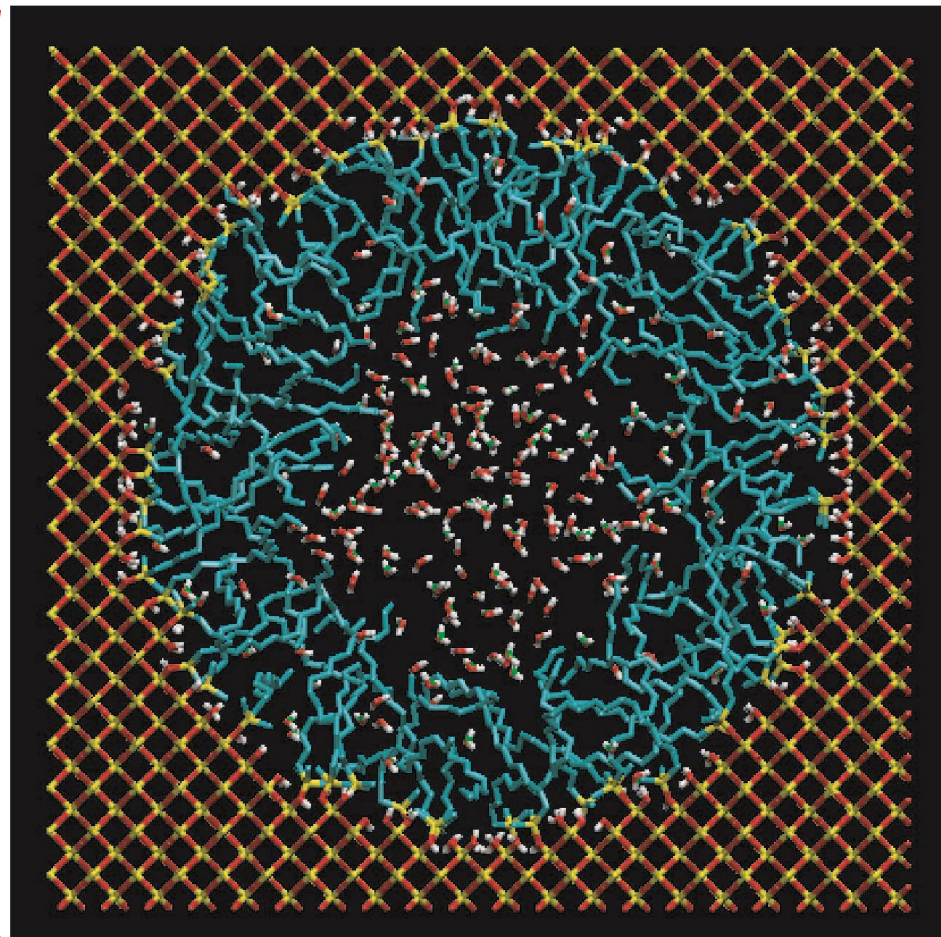
Water is the weakest solvent in RPLC. Organic is stronger solvent.

LC Retention – Part II

Thermodynamics of RPLC



PWC 4101-06 Fig. 2.5 Pore structure of a stationary phase particle. 60-80 Å pores 200-300 m²/g.



Rafferty, Siepmann, Schure, A-Chem, ca. 2007

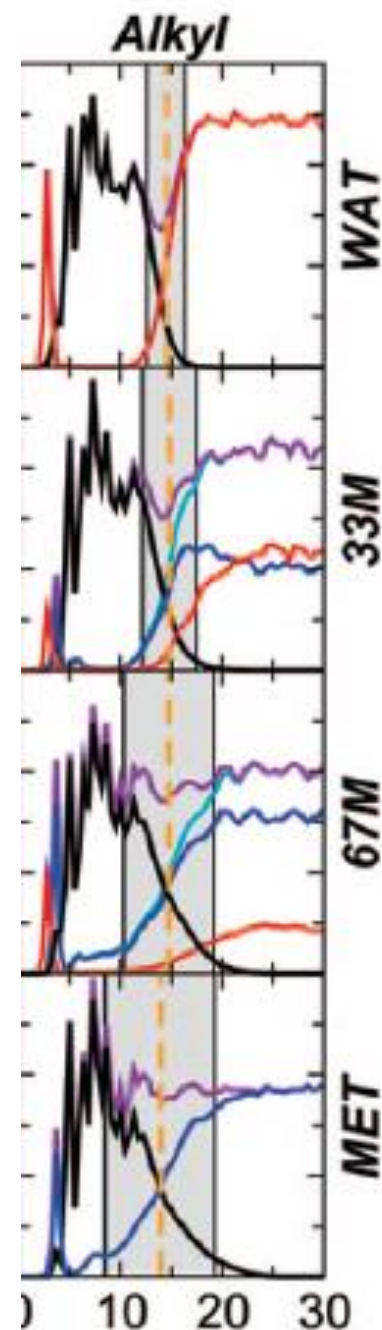
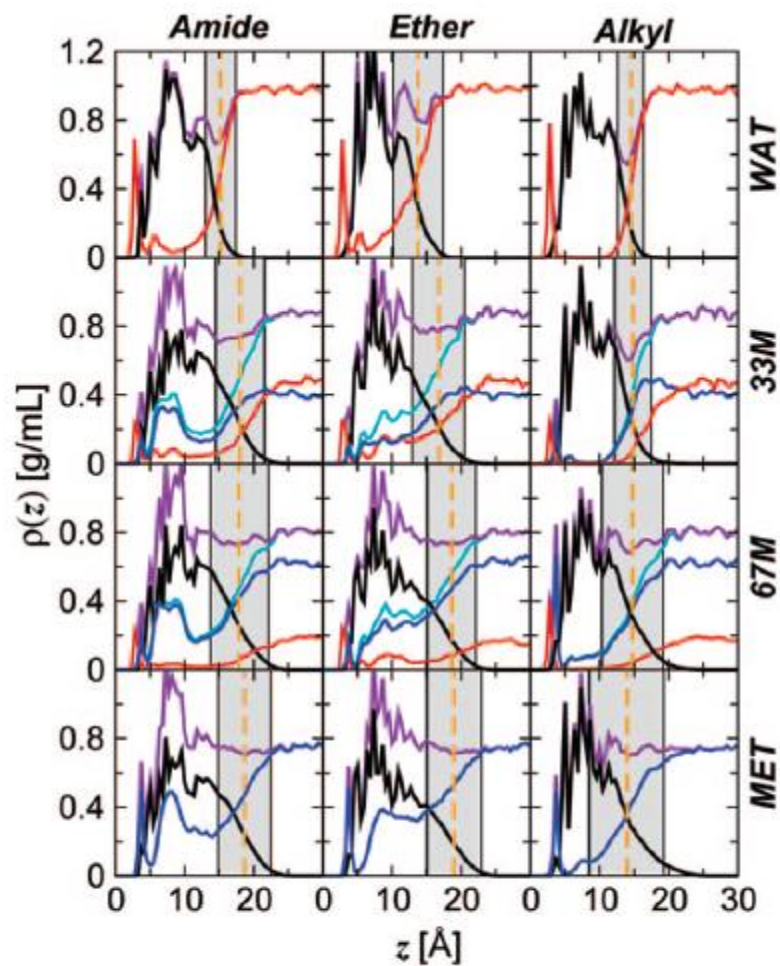


Figure 3. Bonded phase (black, excluding methyl side chains), water (red), methanol (blue), combined solvent (cyan), and total (violet) density profiles. Vertical dashed orange lines denote the Gibbs dividing surface, and the shaded gray area represents the 10–90 interfacial region as defined by the overall solvent density. These and subsequent profiles were computed using a bin width of 0.45 Å.

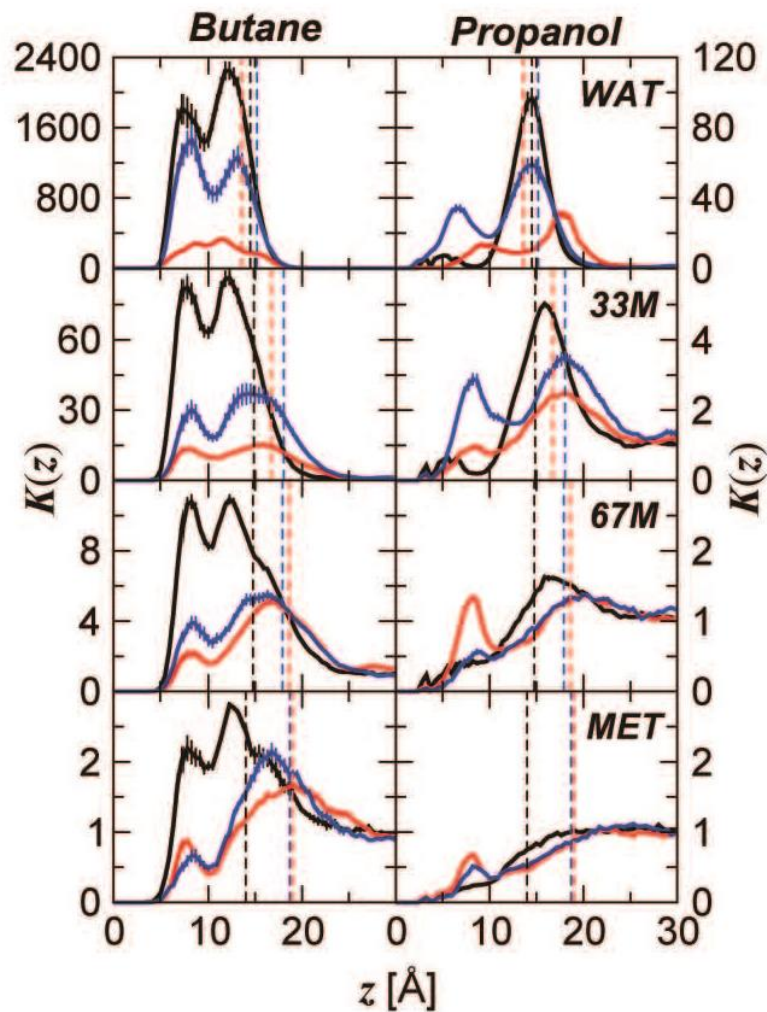
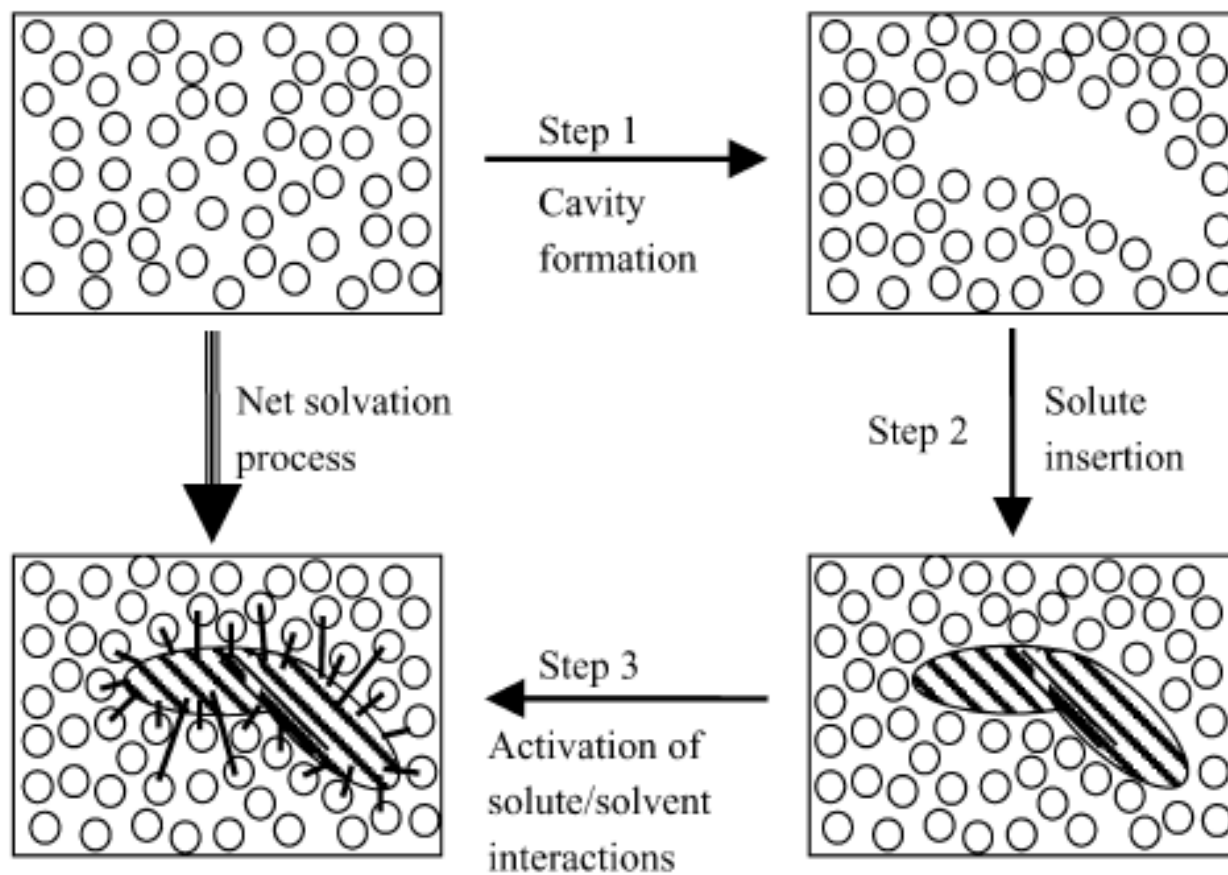


Figure 8. Distribution coefficient profiles for *n*-butane and 1-propanol computed for the transfer from the solvent phase to the box containing the stationary phase (blue, red, and black profiles for amide, ether, and alkyl phase, respectively). Dashed vertical lines denote the GDS.



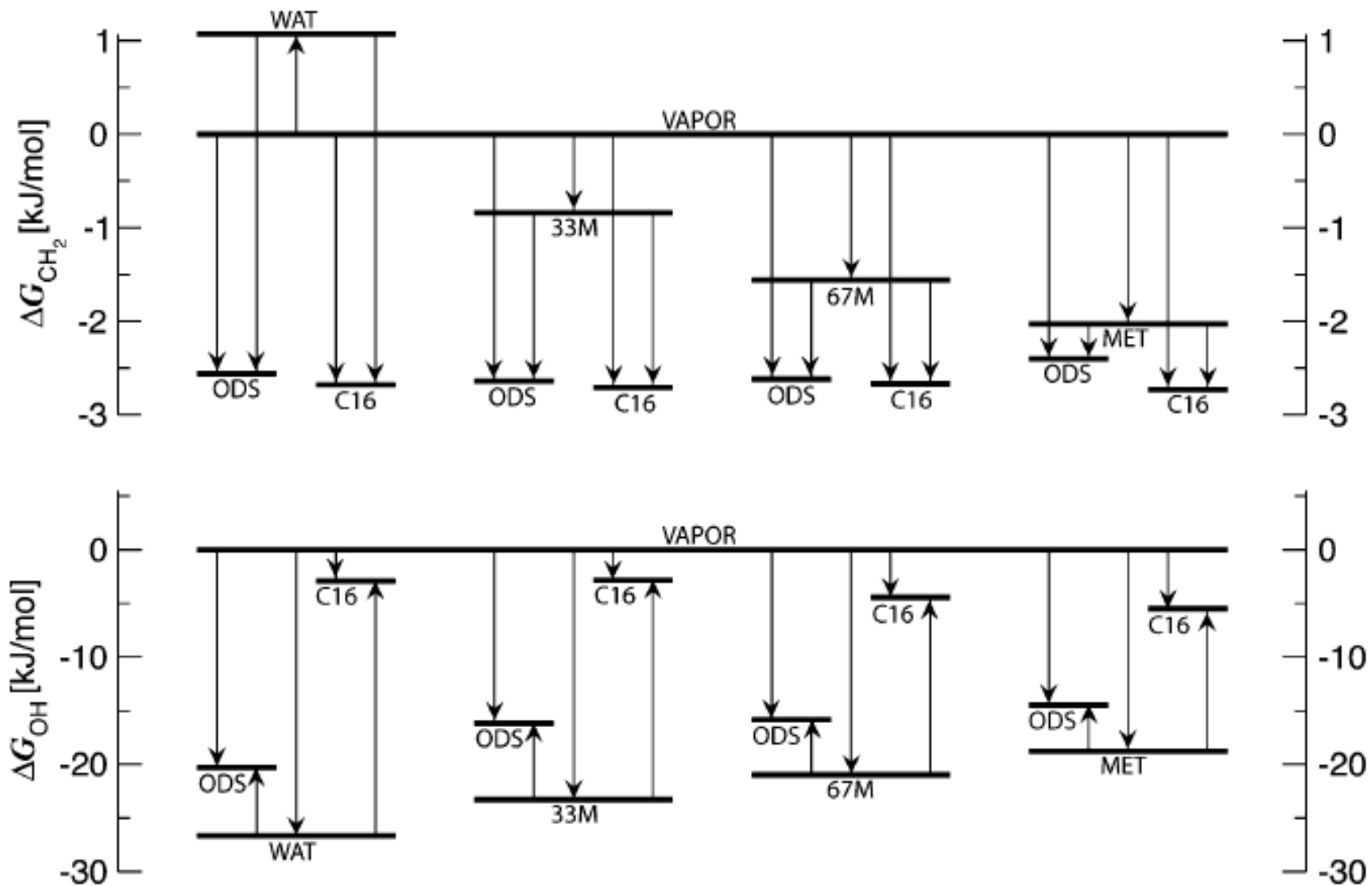


Figure 5. Thermodynamic driving forces for retention. The incremental free energies of transfer for methylene and hydroxyl groups into the stationary phase (ODS), the bulk *n*-hexadecane phase (C16), and the bulk mobile phase (WAT, 33M, 67M, MET) are shown with respect to the ideal gas reference phase (VAPOR)

Table 3.4 Air–Hexadecane, Air–Water, and Hexadecane–Water Equilibrium Partitioning of Hexane, Benzene, Diethylether, and Ethanol: Free Energies, Enthalpies, and Entropies of Transfer, as well as Partition Constants Expressed on a Molar Base (i.e., mol · L⁻¹phase 1/mol · L⁻¹phase 2)

| Phase 1/Phase 2 Compound (<i>i</i>) | $\Delta_{12}G_i$ (kJ · mol ⁻¹) | $\Delta_{12}H_i$ (kJ · mol ⁻¹) | $T\Delta_{12}S_i$ (kJ · mol ⁻¹) | $\Delta_{12}S_i$ (kJ · mol ⁻¹) | K_{i12}^a |
|------------------------------------------|-----------------------------------------------|-----------------------------------------------|------------------------------------------------|-----------------------------------------------|----------------------|
| Air/Hexadecane | | | | | |
| Hexane | 4.2 | 31.0 | 26.8 | 89.9 | 2.2×10^{-3} |
| Benzene | 4.9 | 30.4 | 25.5 | 85.6 | 1.7×10^{-3} |
| Diethylether | 0.8 | 25.2 | 24.4 | 81.9 | 8.7×10^{-3} |
| Ethanol | -2.5 | 16.3 | 18.8 | 73.3 | 3.3×10^{-2} |
| Air/Water | | | | | |
| Hexane | -28.3 | 32.0 | 60.3 | 202.3 | 6.5×10^1 |
| Benzene | -14.1 | 29.7 | 43.8 | 147.0 | 2.1×10^1 |
| Diethylether | -11.2 | 46.8 | 58.8 | 194.6 | 6.6×10^{-2} |
| Ethanol | 3.1 | 52.6 | 49.5 | 166.3 | 2.0×10^{-4} |
| Hexadecane/Water | | | | | |
| Hexane | -32.5 | 1.0 | 33.5 | 112.4 | 3.0×10^4 |
| Benzene | -19.0 | 1.3 | 20.3 | 68.1 | 1.3×10^2 |
| Diethylether | -12.0 | 21.6 | 33.6 | 112.8 | 7.7×10^0 |
| Ethanol | 5.6 | 36.3 | 30.7 | 103.0 | 6.4×10^{-3} |

^a Eq. 3-13 with const. = \bar{V}_1 / \bar{V}_2 ; molar volumes at 25°C and 1 bar: $\bar{V}_{\text{ideal gas}} = 24.73 \text{ L} \cdot \text{mol}^{-1}$, $\bar{V}_{\text{hexadecane}} = 0.293 \text{ L} \cdot \text{mol}^{-1}$, $\bar{V}_{\text{water}} = 0.018 \text{ L} \cdot \text{mol}^{-1}$

LC Retention – Part III

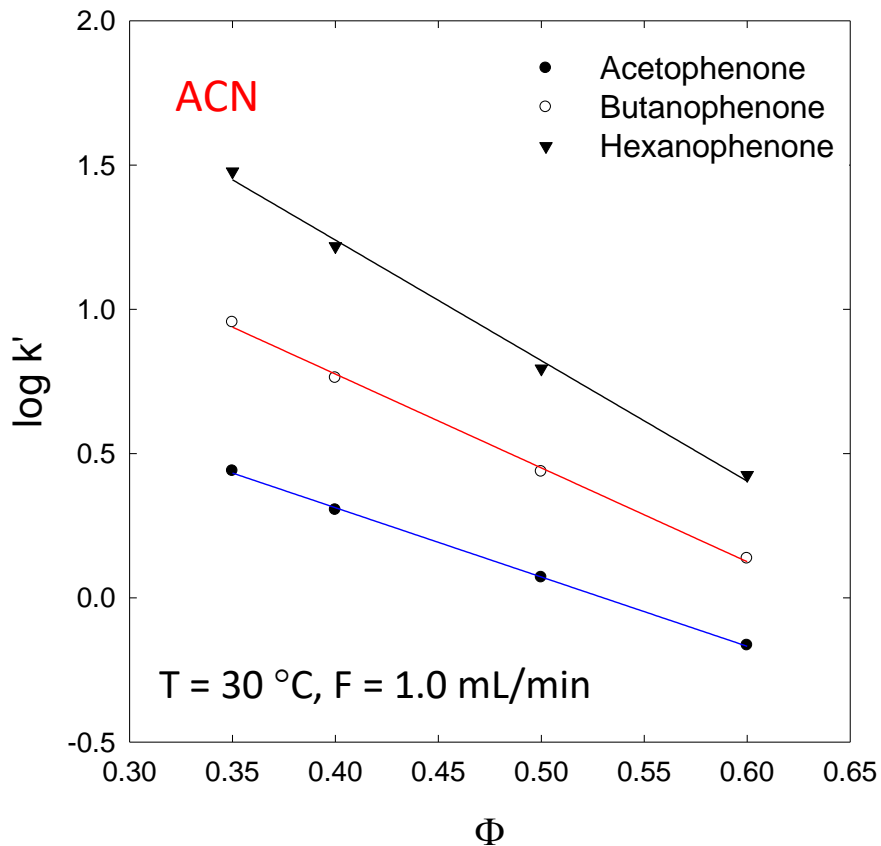
Practical RPLC

| Solvent | Strength ϵ° | Viscosity $\eta(\text{mPa s})$ | Refractive index n_D^{20} | UV cutoff (nm) | Boiling point ($^\circ\text{C}$) | Dipole π^* | Acidity α | Basicity β |
|--------------------------------|------------------------------|-----------------------------------|-----------------------------------|----------------------|------------------------------------------|-------------------|---------------------|---------------------|
| Fluoroalkane FC-78 | -0.19 | 0.4 | 1.267 | 210 | 50 | | | |
| <i>n</i> -Pentane | 0.00 | 0.23 | 1.3575 | 195 | 36 | | | |
| <i>n</i> -Hexane | 0.00 | 0.33 | 1.3749 | 190 | 69 | | | |
| Isooctane | 0.01 | 0.50 | 1.3914 | 200 | 99 | | | |
| Cyclohexane* | 0.03 | 1.00 | 1.4262 | 200 | 81 | | | |
| Cyclopentane | 0.04 | 0.47 | 1.4064 | 200 | 49 | | | |
| Carbon tetrachloride | 0.14 | 0.97 | 1.4652 | 265 | 77 | | | |
| <i>p</i> -Xylene | 0.20 | 0.62 | 1.4958 | 290 | 138 | 0.81 | 0.00 | 0.19 |
| Diisopropyl ether | 0.22 | 0.37 | 1.3681 | 220 | 68 | 0.36 | 0.00 | 0.64 |
| Toluene | 0.22 | 0.59 | 1.4969 | 285 | 111 | 0.83 | 0.00 | 0.17 |
| Chlorobenzene | 0.23 | 0.80 | 1.5248 | 290 | 132 | 0.91 | 0.00 | 0.09 |
| Benzene | 0.25 | 0.65 | 1.5011 | 280 | 80 | 0.86 | 0.00 | 0.14 |
| Diethyl ether | 0.29 | 0.24 | 1.3524 | 205 | 34.5 | 0.36 | 0.00 | 0.64 |
| Dichloromethane | 0.30 | 0.44 | 1.4242 | 230 | 40 | 0.73 | 0.27 | 0.00 |
| Chloroform | 0.31 | 0.57 | 1.4457 | 245 | 61 | 0.57 | 0.43 | 0.00 |
| 1,2-Dichloroethane | 0.38 | 0.79 | 1.4448 | 230 | 83 | 1.00 | 0.00 | 0.00 |
| Triethylamine | 0.42 | 0.38 | 1.4010 | 230 | 89 | 0.16 | 0.00 | 0.84 |
| Acetone | 0.43 | 0.32 | 1.3587 | 330 | 56 | 0.56 | 0.06 | 0.38 |
| Dioxane | 0.43 | 1.54 | 1.4224 | 220 | 101 | 0.60 | 0.00 | 0.40 |
| Methyl acetate | 0.46 | 0.37 | 1.3614 | 260 | 56 | 0.55 | 0.05 | 0.40 |
| Tetrahydrofuran | 0.48 | 0.46 | 1.4072 | 220 | 66 | 0.51 | 0.00 | 0.49 |
| <i>tert.</i> Butylmethyl ether | 0.48 | 0.35 | 1.3689 | 220 | 53 | 0.36 | 0.00 | 0.64 |
| Ethyl acetate | 0.48 | 0.45 | 1.3724 | 260 | 77 | 0.55 | 0.00 | 0.45 |
| Dimethyl sulphoxide | 0.48 | 2.24 | 1.4783 | 270 | 189 | 0.57 | 0.00 | 0.43 |
| Nitromethane | 0.49 | 0.67 | 1.3819 | 380 | 101 | 0.64 | 0.17 | 0.19 |
| Acetonitrile | 0.50 | 0.37 | 1.3441 | 190 | 82 | 0.60 | 0.15 | 0.25 |
| Pyridine | 0.55 | 0.94 | 1.5102 | 305 | 115 | 0.58 | 0.00 | 0.42 |
| Isopropanol | 0.60 | 2.3 | 1.3772 | 210 | 82 | 0.22 | 0.35 | 0.43 |
| Ethanol | 0.68 | 1.20 | 1.3614 | 210 | 78 | 0.25 | 0.39 | 0.36 |
| Methanol | 0.73 | 0.60 | 1.3284 | 205 | 65 | 0.28 | 0.43 | 0.29 |
| Acetic acid | High | 1.26 | 1.3719 | 260 | 118 | 0.31 | 0.54 | 0.15 |
| Water | Higher | 1.00 | 1.3330 | <190 | 100 | 0.39 | 0.43 | 0.18 |
| Salt solutions, buffers | Highest | | | | | | | |

* Becomes solid at 350 bar!

Linear Solvent Strength Characterization

$$\log k' = \log k'_w - S\phi$$

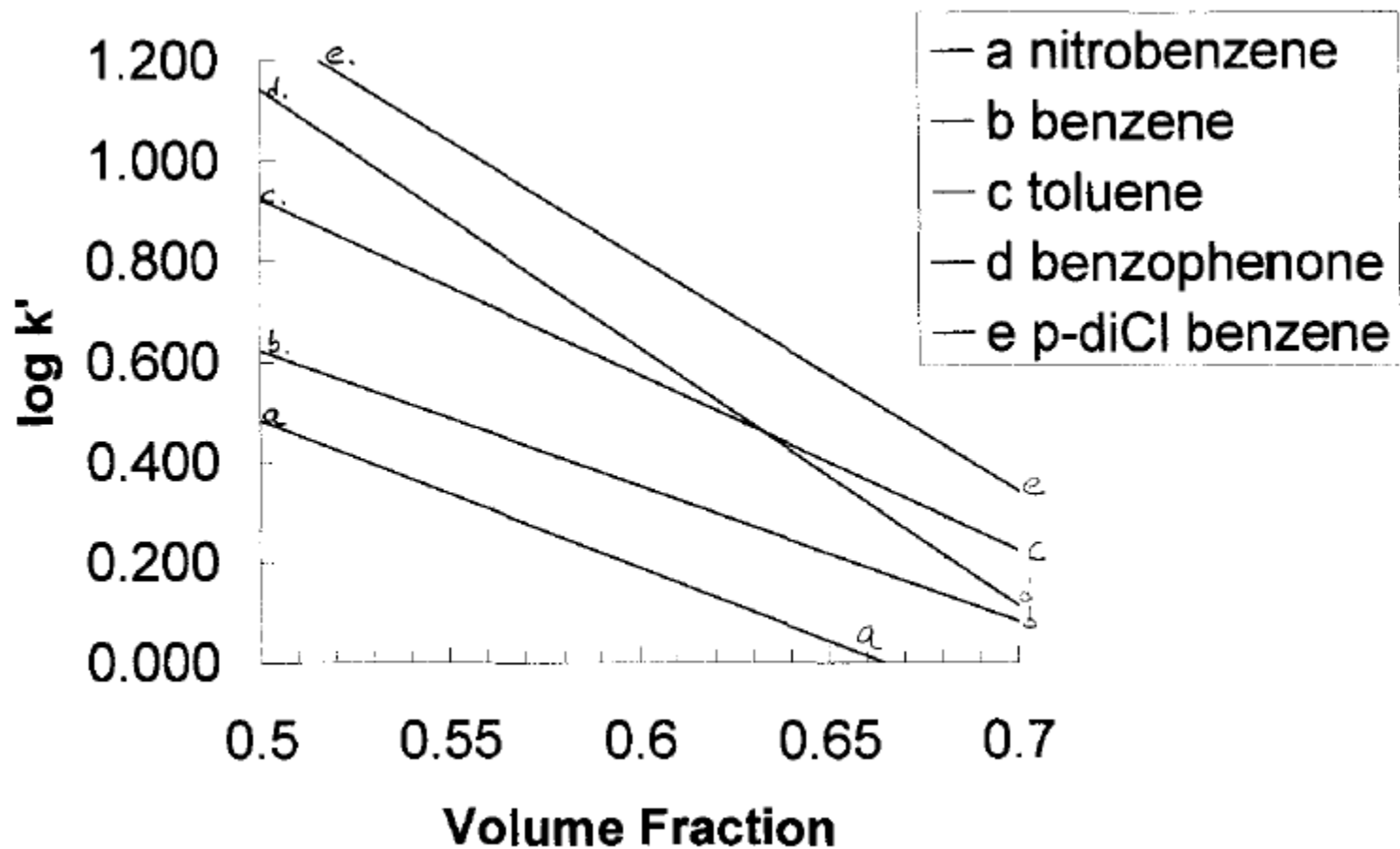


Calculated S Values

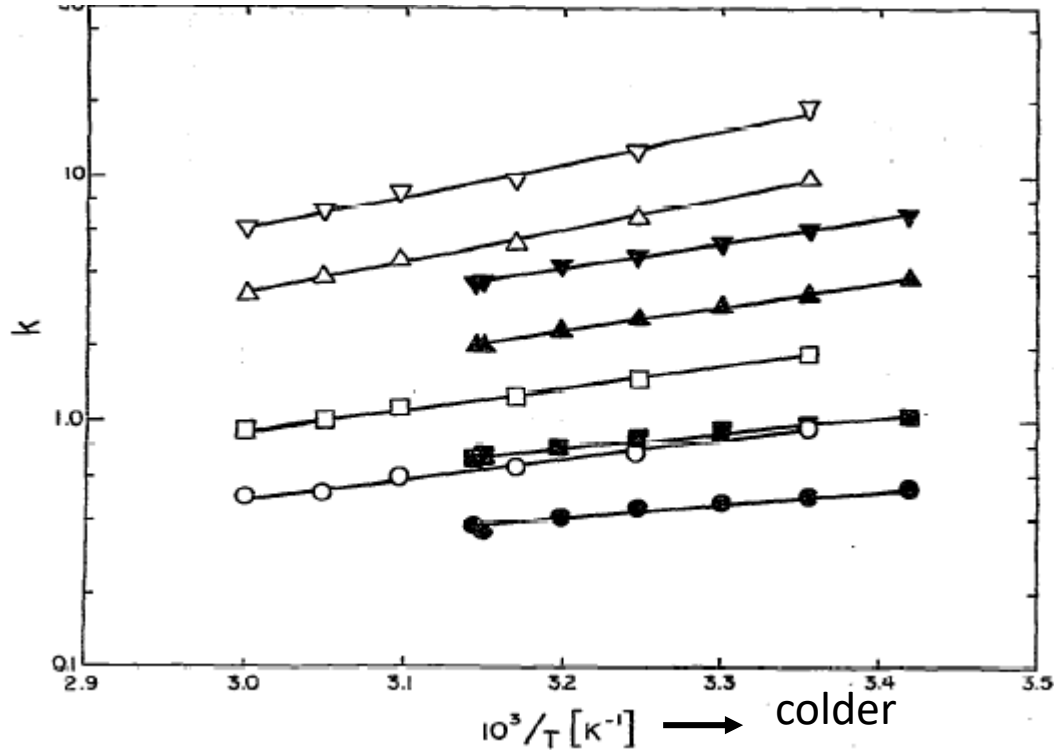
| | ACN | CH ₃ OH | THF |
|----|-----------------|--------------------|-----------------|
| AP | 2.40 ± 0.04 | 2.60 ± 0.01 | 2.76 ± 0.07 |
| BP | 3.25 ± 0.10 | 3.53 ± 0.01 | 4.11 ± 0.13 |
| HP | 4.18 ± 0.18 | 4.52 ± 0.02 | 5.70 ± 0.24 |

The highly crosslinked C8 phase behaves as a typical **reversed phase** material

Effect of Volume Fraction of Methanol

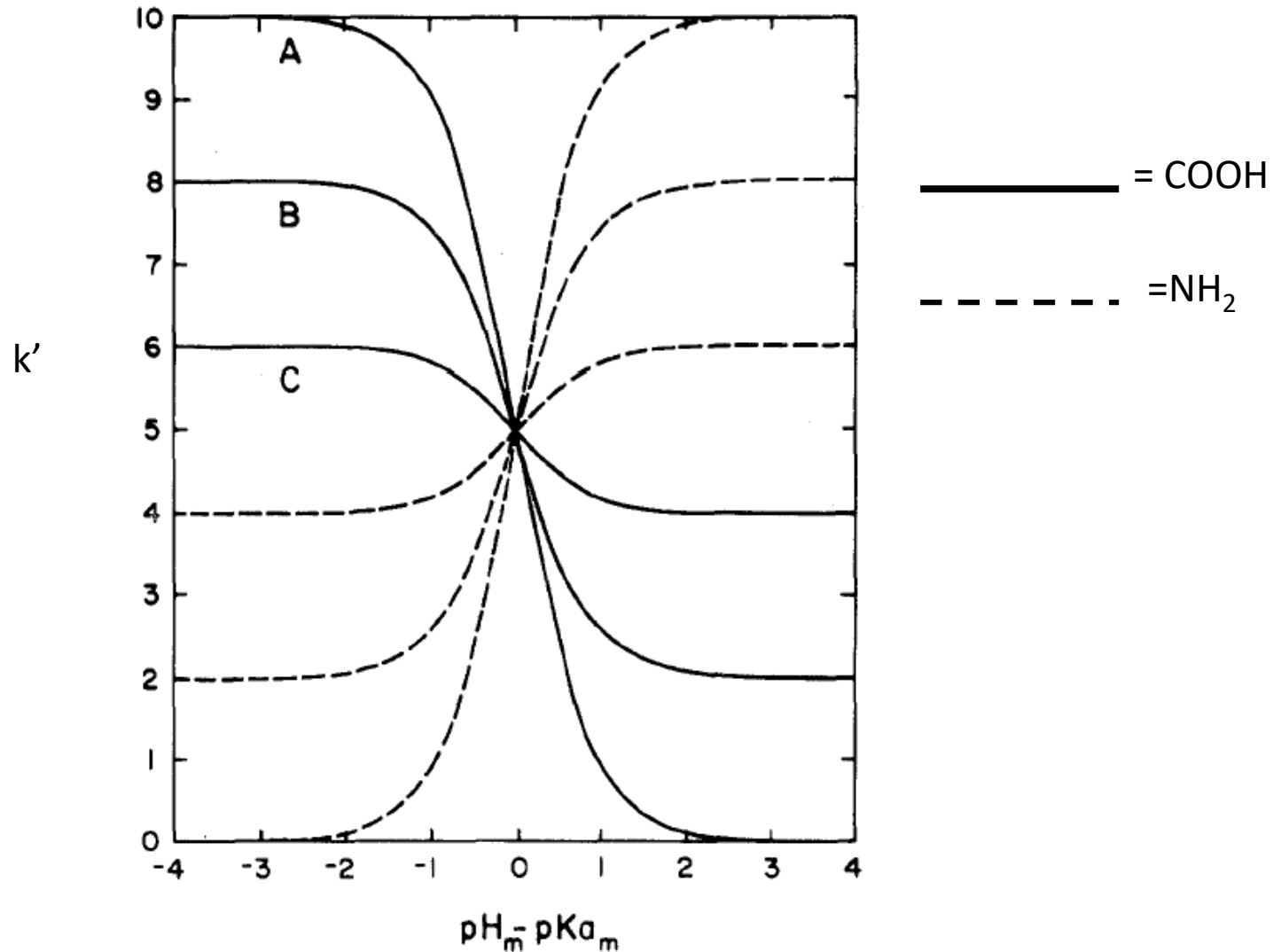


Effect of Temperature

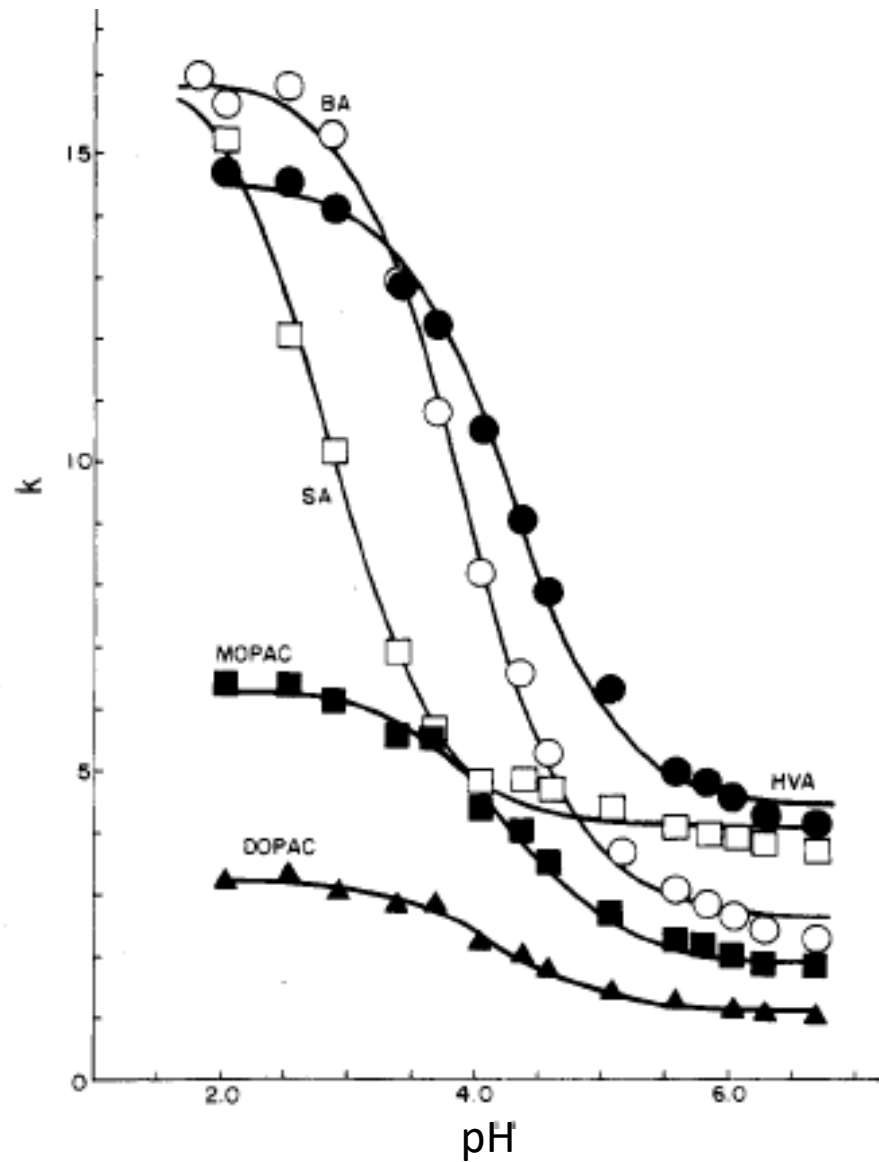


50 °C = 2-3 in k'

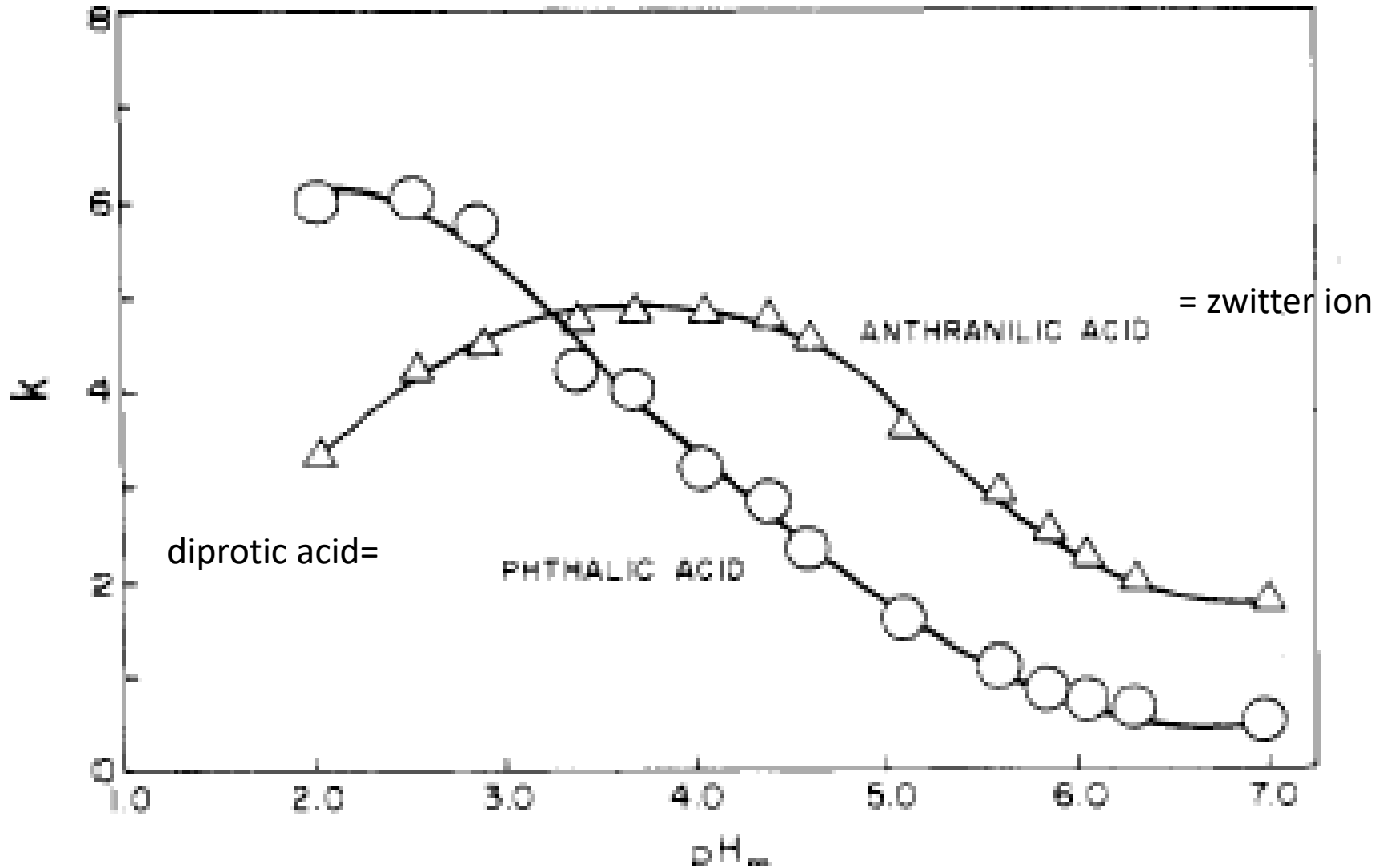
Effect of pH on k'



pH Effect on Monoprotic Acids

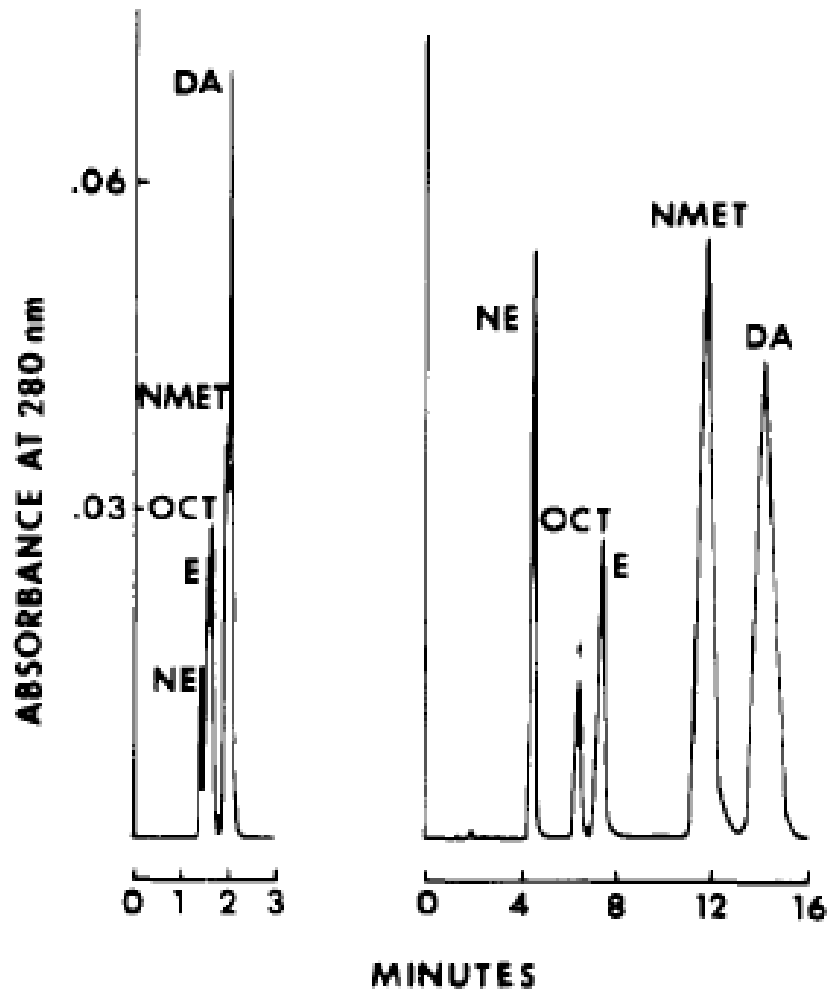


pH Effect on Diprotic and Zwitter Ions



Effect of ion-pairing on RP retention

Effect of Adding 3mM Octylsulfate on Catecholamines



Typical RP-Product Line

Several Pore Sizes

⇒ 60 Å, 120 Å, 200 Å, 300 Å

Several Particle Sizes

⇒ 3µm, 5µm, 10µm, 15µm, 20µm

Several Bonding Types

⇒ C1, CN, C4, Phenyl, C8, C18, C30

Several Bonding Chemistries

⇒ end capped, non end capped, polar embedded,
aqueous compatible

No Metal Impurities

Properties of RP-Packings

⇒ **Hydrophobicity**

surface area

bonding type

bonding chemistry

⇒ **Silanophilic Activity**

bonding chemistry

⇒ **Shape Selectivity**

bonding chemistry

⇒ **Polar Selectivity**

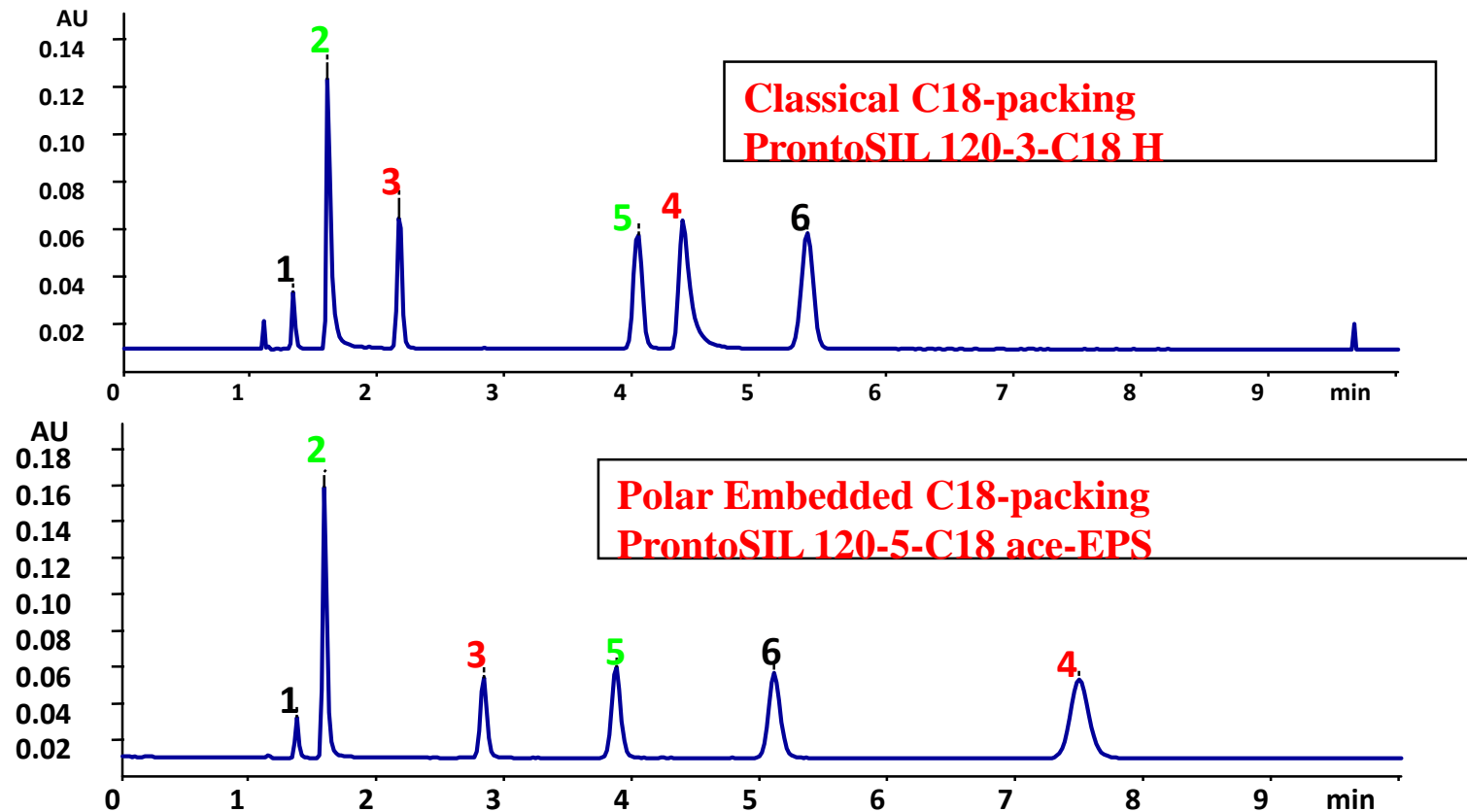
bonding chemistry

⇒ **Metal Content**

manufacturing of the silica

Comparison of Selectivities

Acidic, basic and neutral compounds



Eluent: ACN/50mM Phosphate buffer pH 3.2 65:35 (v/v)
Flow: 1.0 ml/min
Temperature: ambient
Injection: 5 μ l
Detection: UV 254 nm
Sample: 1 Uracil, 2 Pyridine, 3 Phenol, 4 p-Butylbenzoic acid, 5 N,N-Dimethylaniline, 6 Toluene

Peak Broadening in Separations in Four Parts
Stoll, CHE380

Objectives for our Discussion of Separations

Basics

1. Define, understand, and use key terms such as retention time, retention factor, selectivity, and resolution.
2. Predict changes in separation metrics upon a change in conditions (e.g., column length, particle size, flow rate, etc.).

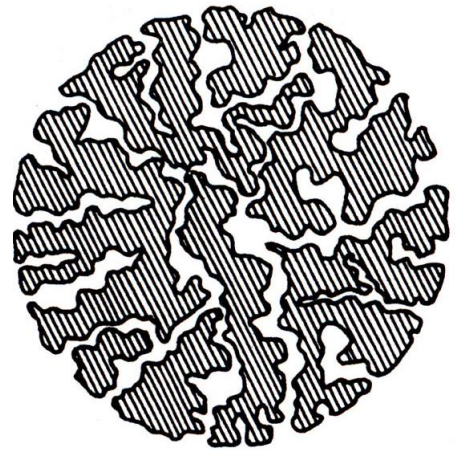
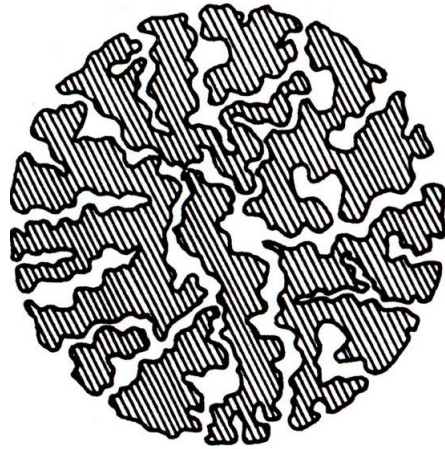
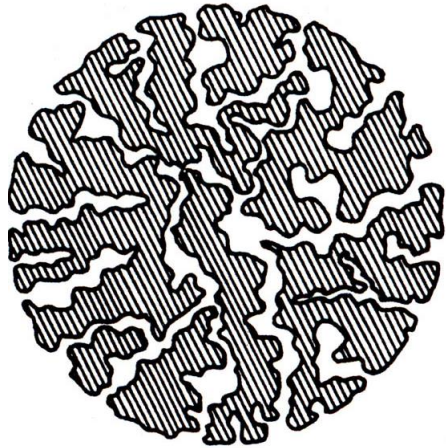
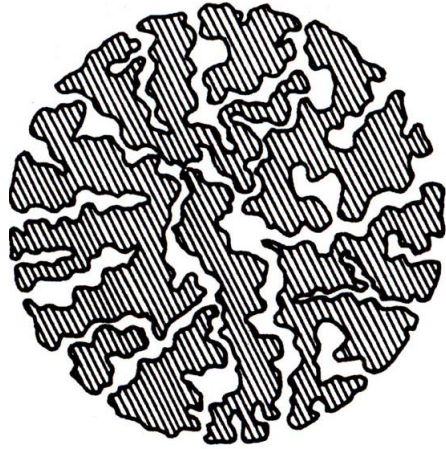
Retention

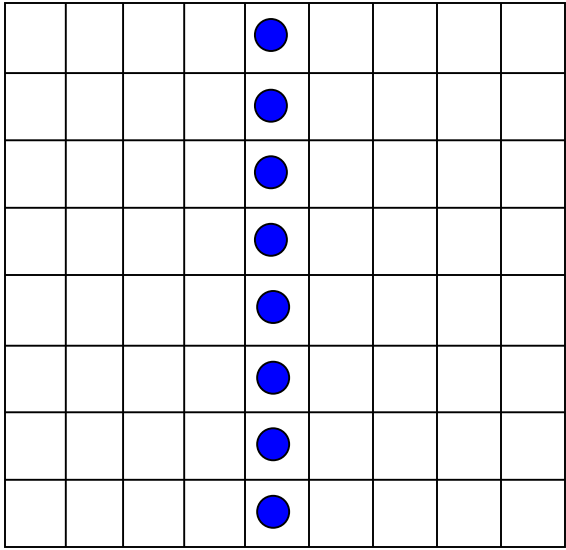
1. (GC/LC) Predict the effect of a change in conditions on relative retention (e.g., change in stationary phase, mobile phase, flow rate, etc.).
2. (GC/LC) Use chemical and physical reasoning to explain the basis of retention, given a specific scenario (e.g., why is benzyl alcohol less retained than benzene in RPLC?).

Peak Broadening

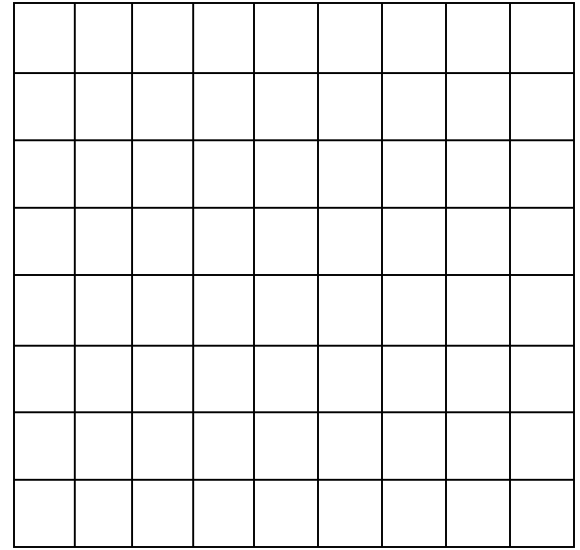
1. (GC/LC) Predict the effect of a change in conditions (e.g., mobile phase type, temperature, particle size, etc.) on peak properties (e.g., height, width, retention time).
2. (GC/LC) Use chemical and physical reasoning to explain the basis of peak broadening, given a specific scenario (e.g., why is the peak for anthracene broader than the peak for benzene under RPLC conditions?).

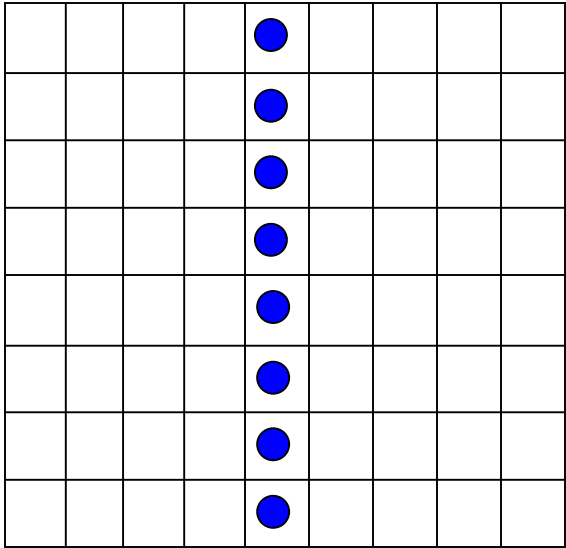
**Part I – Diffusion, Convection, and
the Physics of Flow through
Chromatography Columns**



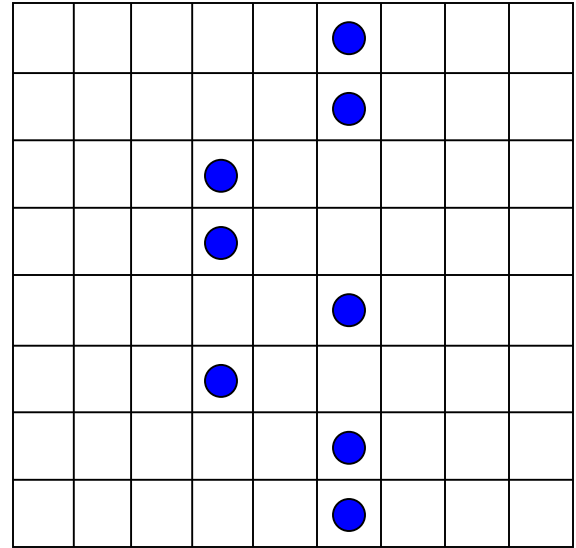


Initial Condition

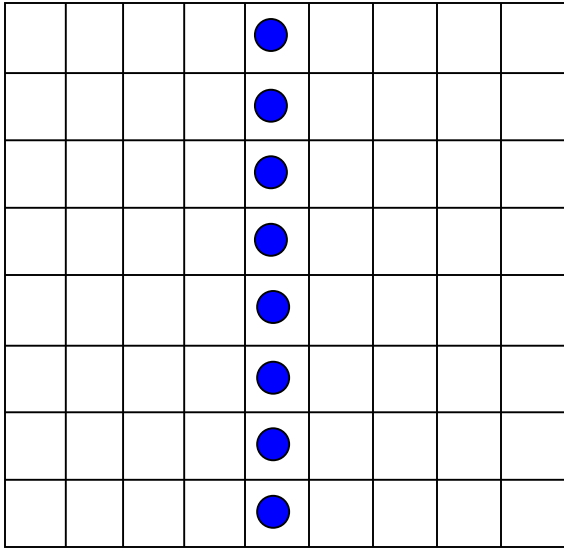




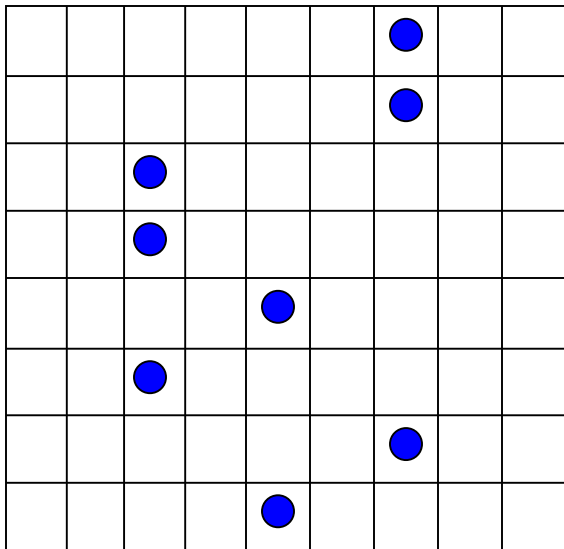
Initial Condition



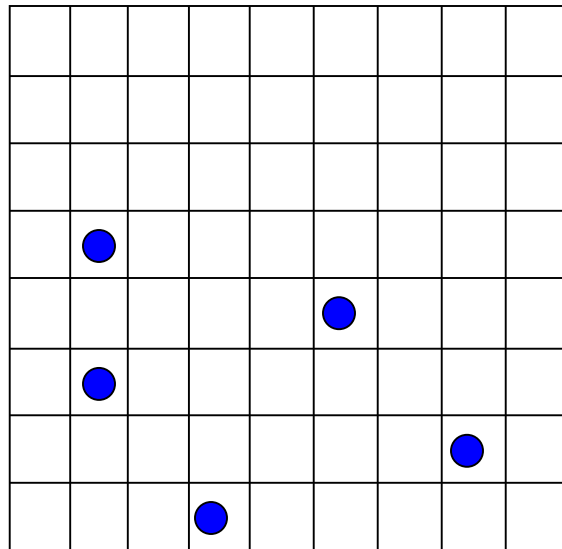
After Step 1



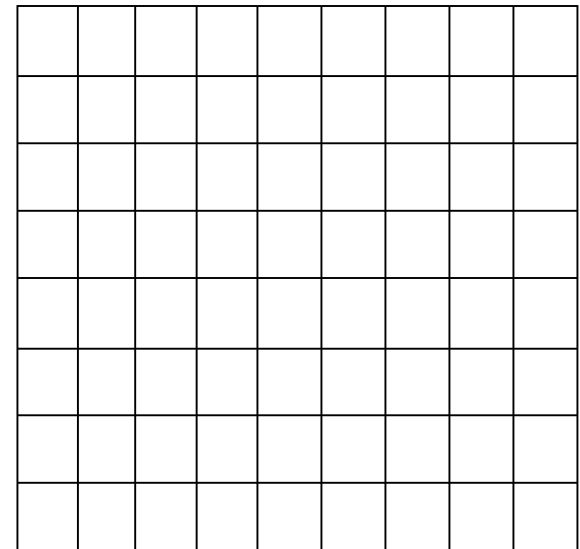
Initial Condition



After Step 2



After Step 3



After Step 4

**INVESTIGATIONS ON
THE THEORY OF ,THE
BROWNIAN MOVEMENT**

BY

ALBERT EINSTEIN, PH.D.

EDITED WITH NOTES BY

R. FÜRTH

TRANSLATED BY

A. D. COWPER

1905

WITH 3 DIAGRAMS

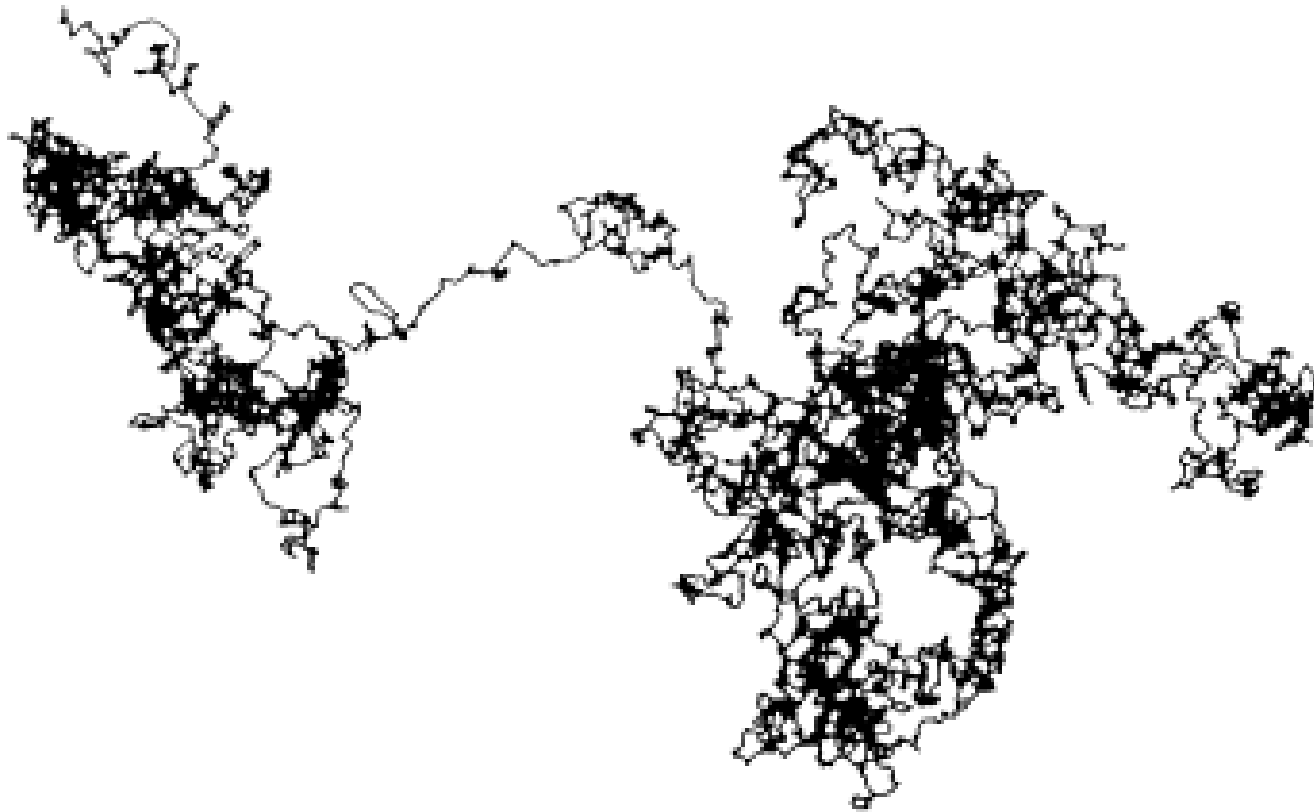


Fig. 1.4. An x, y plot of a two-dimensional random walk of $n = 18,050$ steps. The computer pen started at the upper left corner of the track and worked its way to the upper right edge of the track. It repeatedly traversed regions that are completely black. It moved, as the crow flies, 196 step lengths. The expected root-mean-square displacement is $(2n)^{1/2} = 190$ step lengths.

Part II – Peak Broadening in Gas Chromatography

The Equation for H in Open Tubular Chromatography (LC or GC, no particles)

$$H_{total} = \frac{(1 + 6k' + 11k'^2)}{(1 + k')^2} \frac{R^2 u_m}{D_m} + \frac{2D_m}{u_m} + \frac{2}{3} \frac{k'}{(1 + k')^2} \frac{d_f^2 u_m}{D_s}$$

$u_m = L/t_m$ – mobile phase velocity (cm/s)

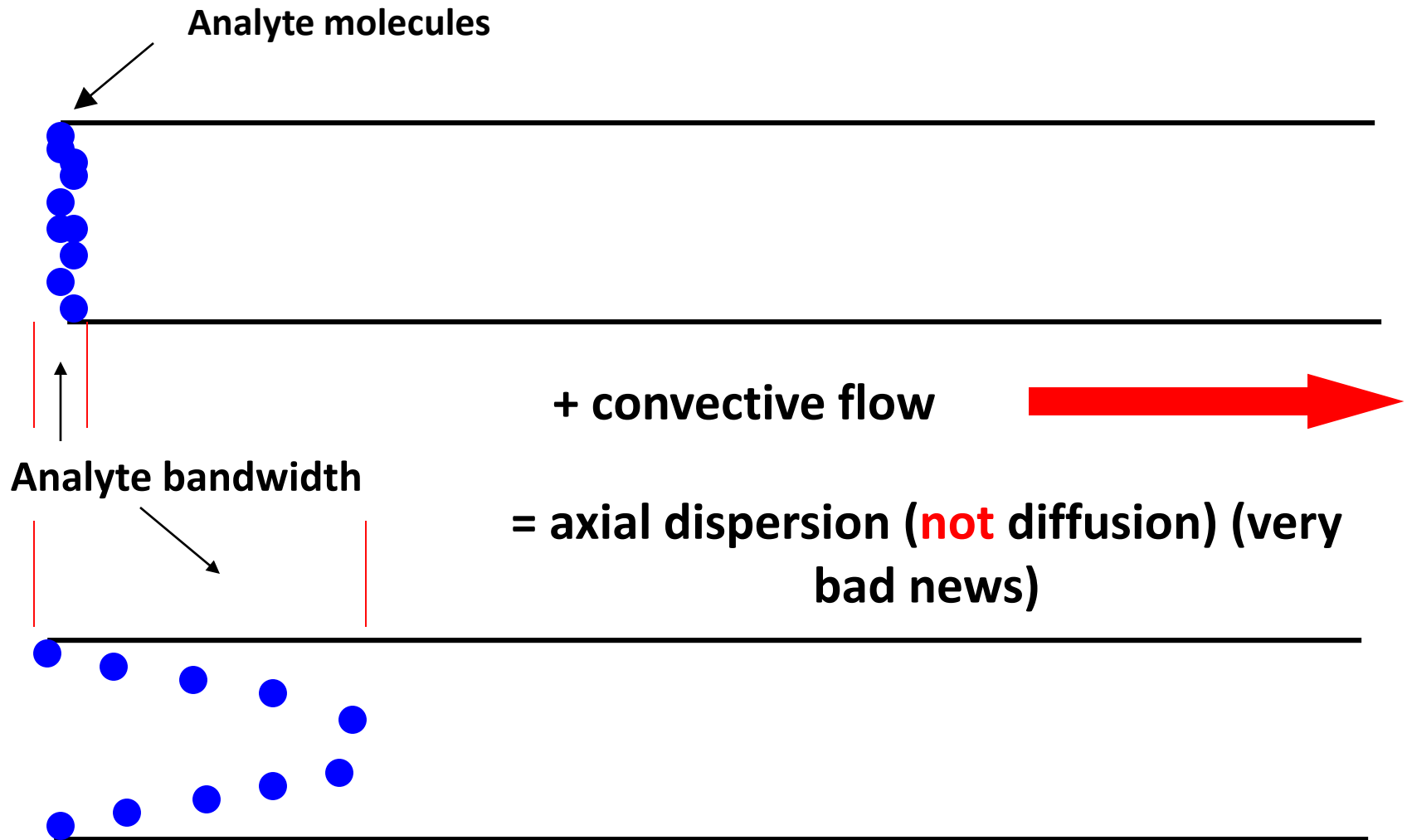
D_m = diffusion coefficient of the analyte in the mobile phase

R = radius of the open tubular column

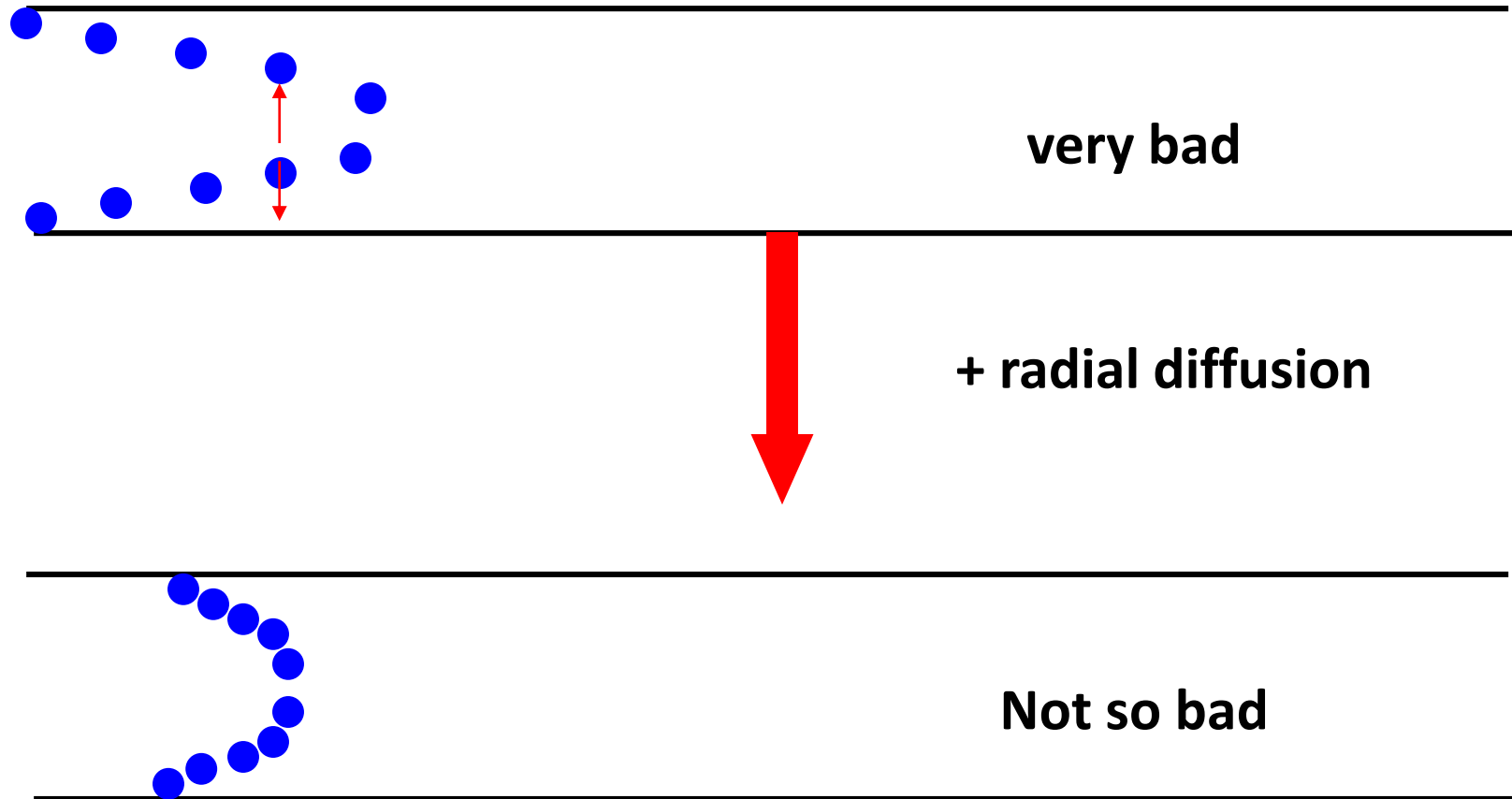
d_f = thickness of the stationary phase film

D_s = diffusion coefficient of the analyte in the stationary phase

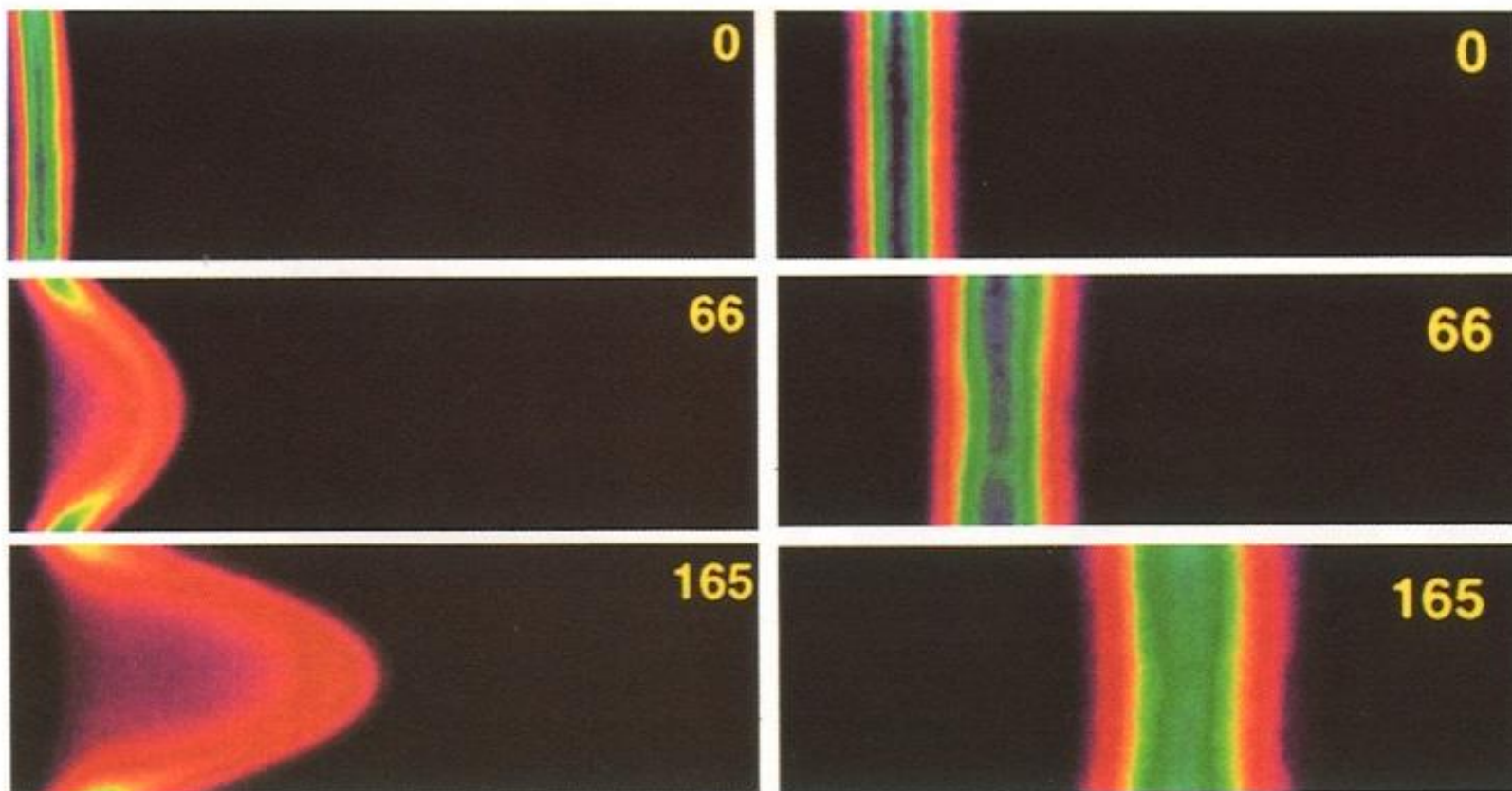
Effect of convective (laminar) flow on analyte bandwidth in an **open tube**



...but, radial **diffusion** saves the day



$$H_{axial} = \frac{(1 + 6k' + 11k'^2)}{(1 + k')^2} \frac{R^2 u_m}{D_m}$$

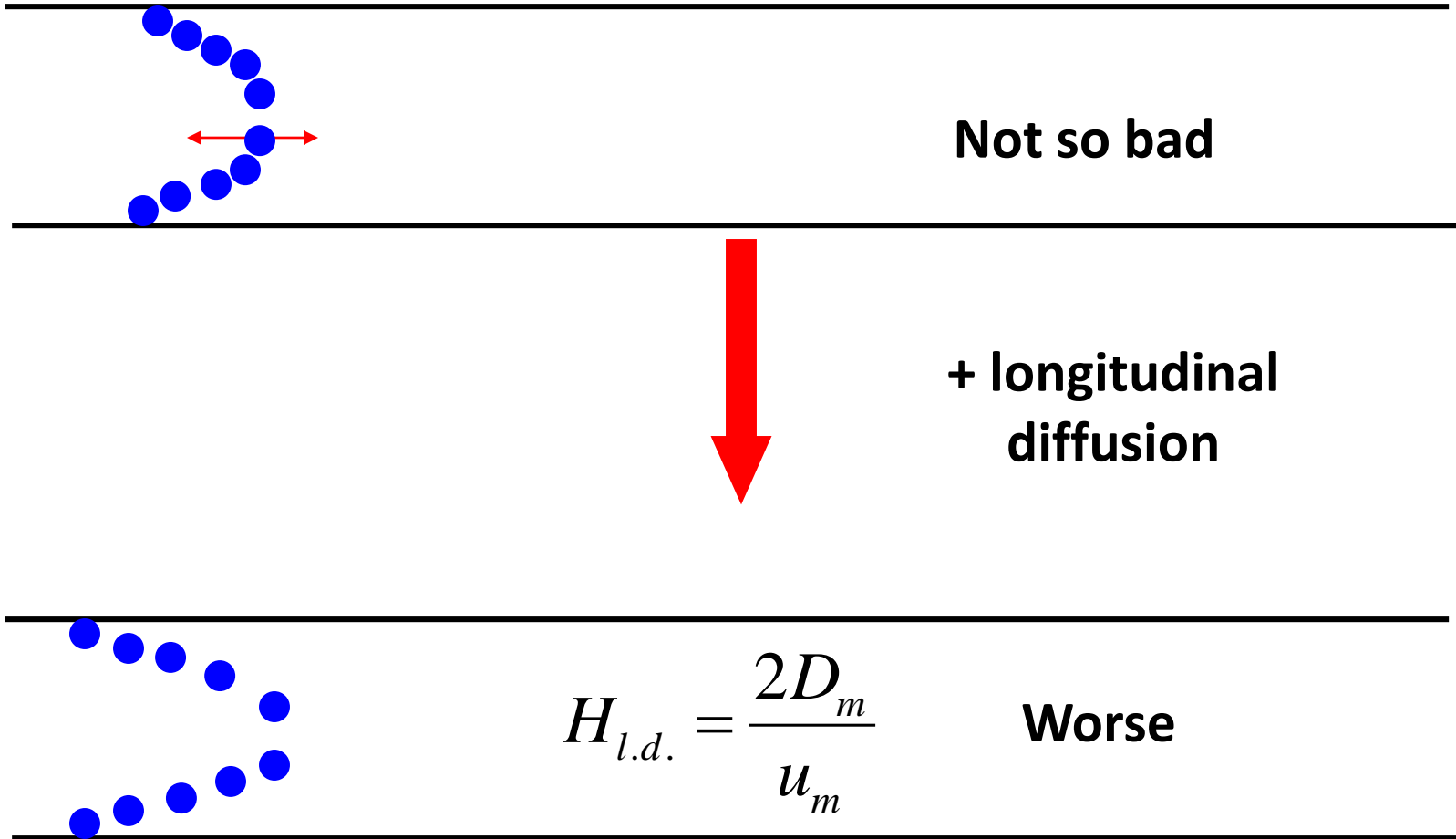


Hydrodynamic flow →
100-μm-diameter capillary

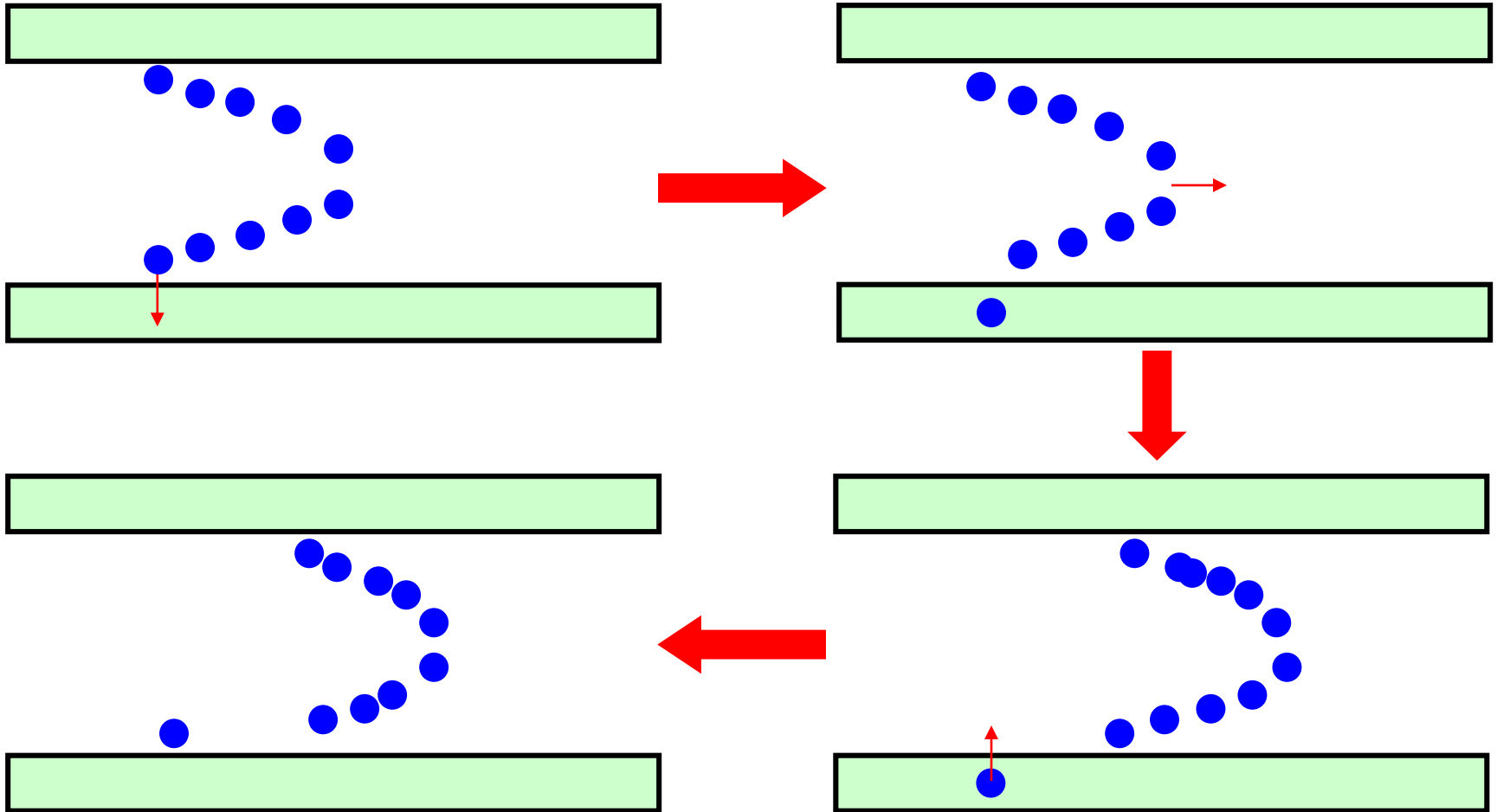
Electroosmotic flow →
75-μm-diameter capillary

Color Plate 30 Velocity Profiles for Hydrodynamic and Electroosmotic Flow (Section 25-6) A fluorescent dye was imaged inside a capillary tube at times 0, 66, and 165 ms after initiating flow. The highest concentration of dye is represented by blue and the lowest concentration is red in these images in which different colors are assigned to different fluorescence intensities. [From P. H. Paul, M. G. Garguilo, and D. J. Rakestraw, *Anal. Chem.* **1998**, *70*, 2459. See also D. Ross, T. J. Johnson, and L. E. Locascio, *Anal. Chem.* **2001**, *73*, 2509.]

longitudinal **diffusion** adds to the problem

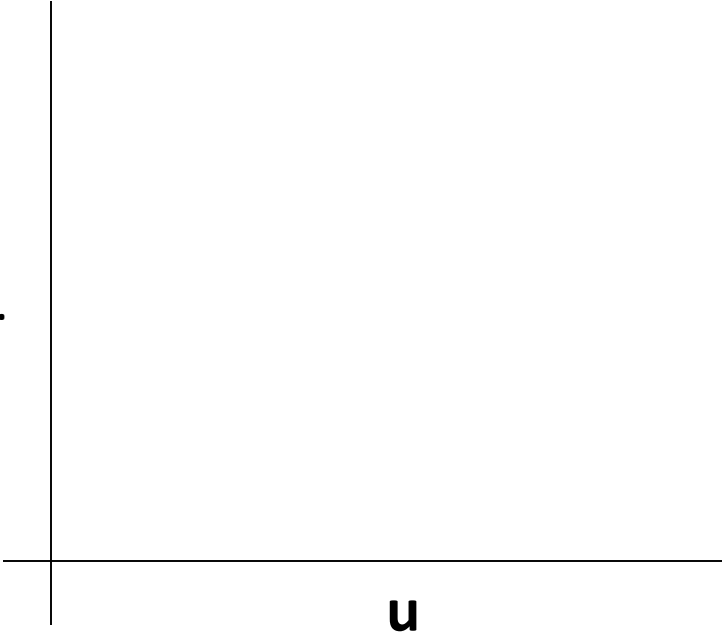


And finally...slow **diffusion** out of the stationary phase...

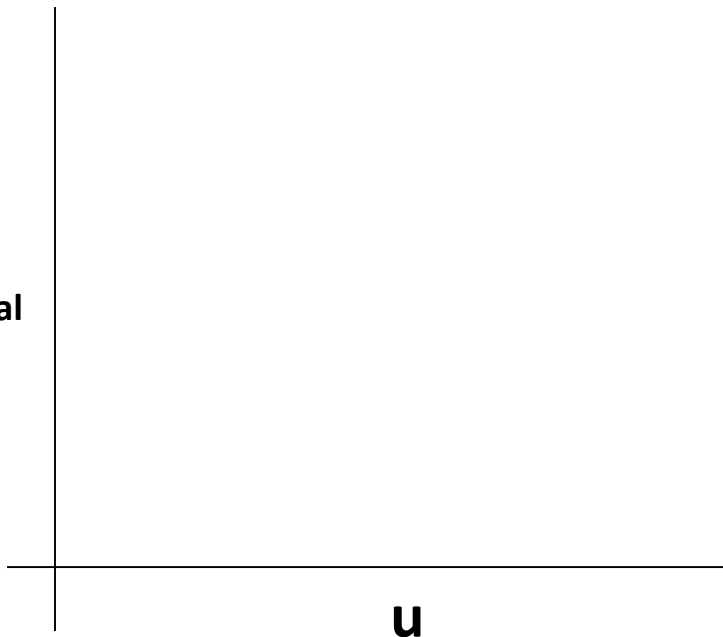


$$H_{s.p.} = \frac{2}{3} \frac{k'}{(1+k')^2} \frac{d_f^2 u_m}{D_s}$$

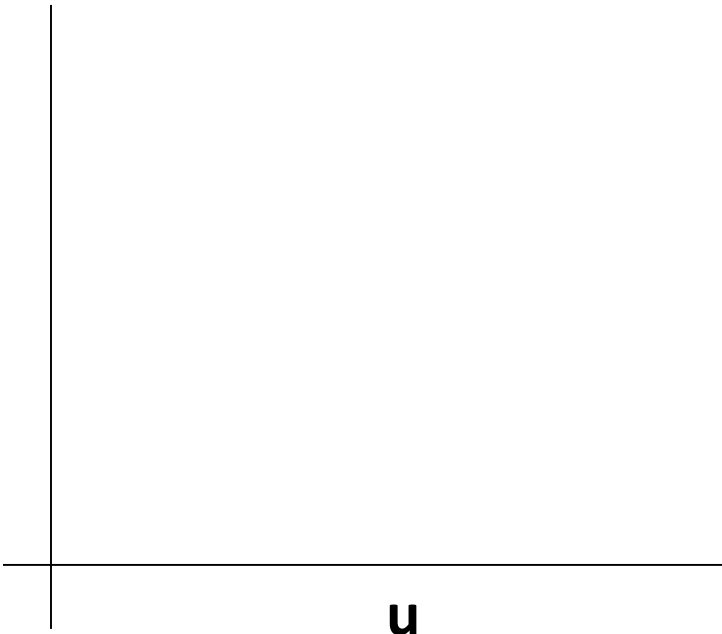
$H_{l.d.}$



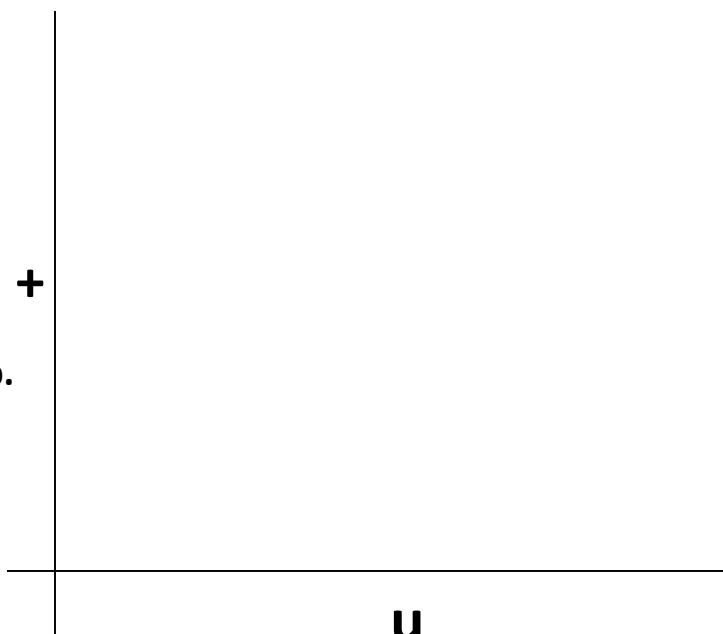
H_{axial}



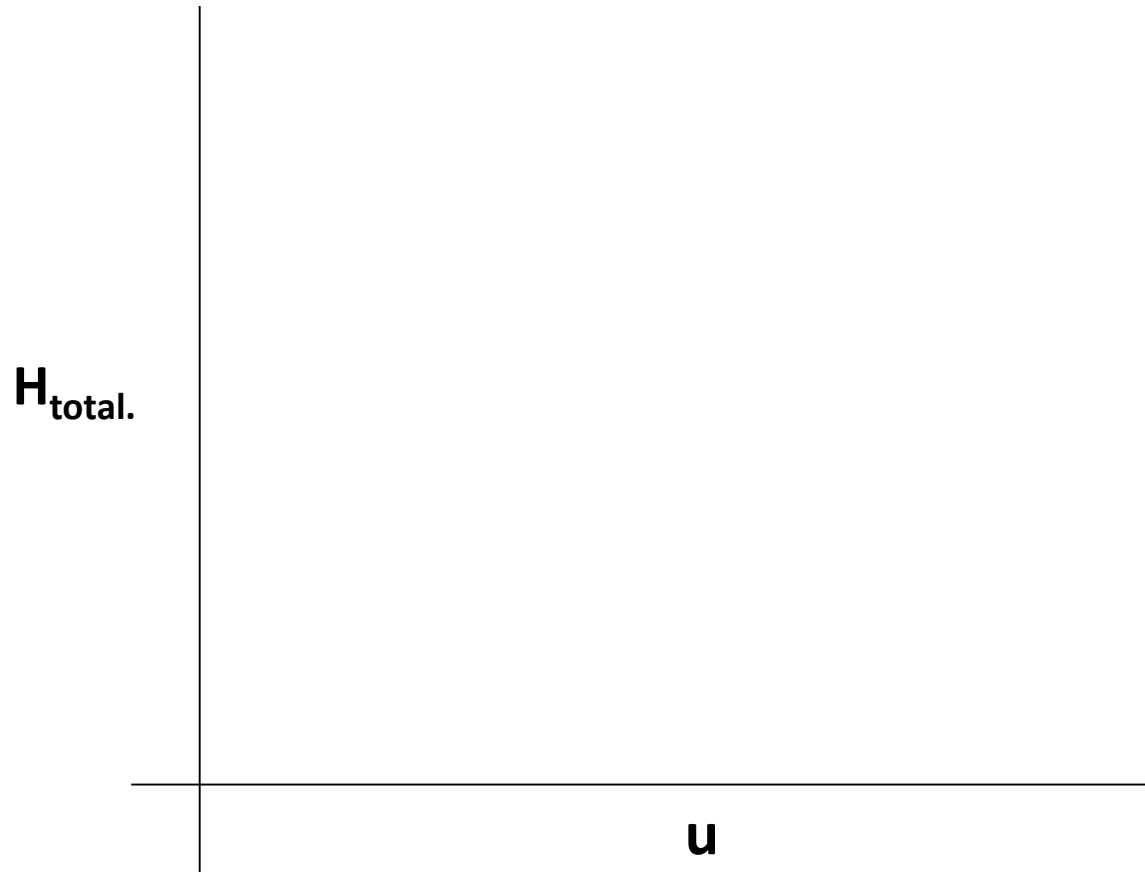
$H_{s.p.}$



$H_{axial} +$
 $H_{s.p.}$



How Does H Depend on u??



For Open Tubular Columns

| | To Make H Small... | Practical Consequence/Problem |
|-------------|--------------------|-------------------------------|
| H_{axial} | | |
| $H_{l.d.}$ | | |
| $H_{s.p.}$ | | |

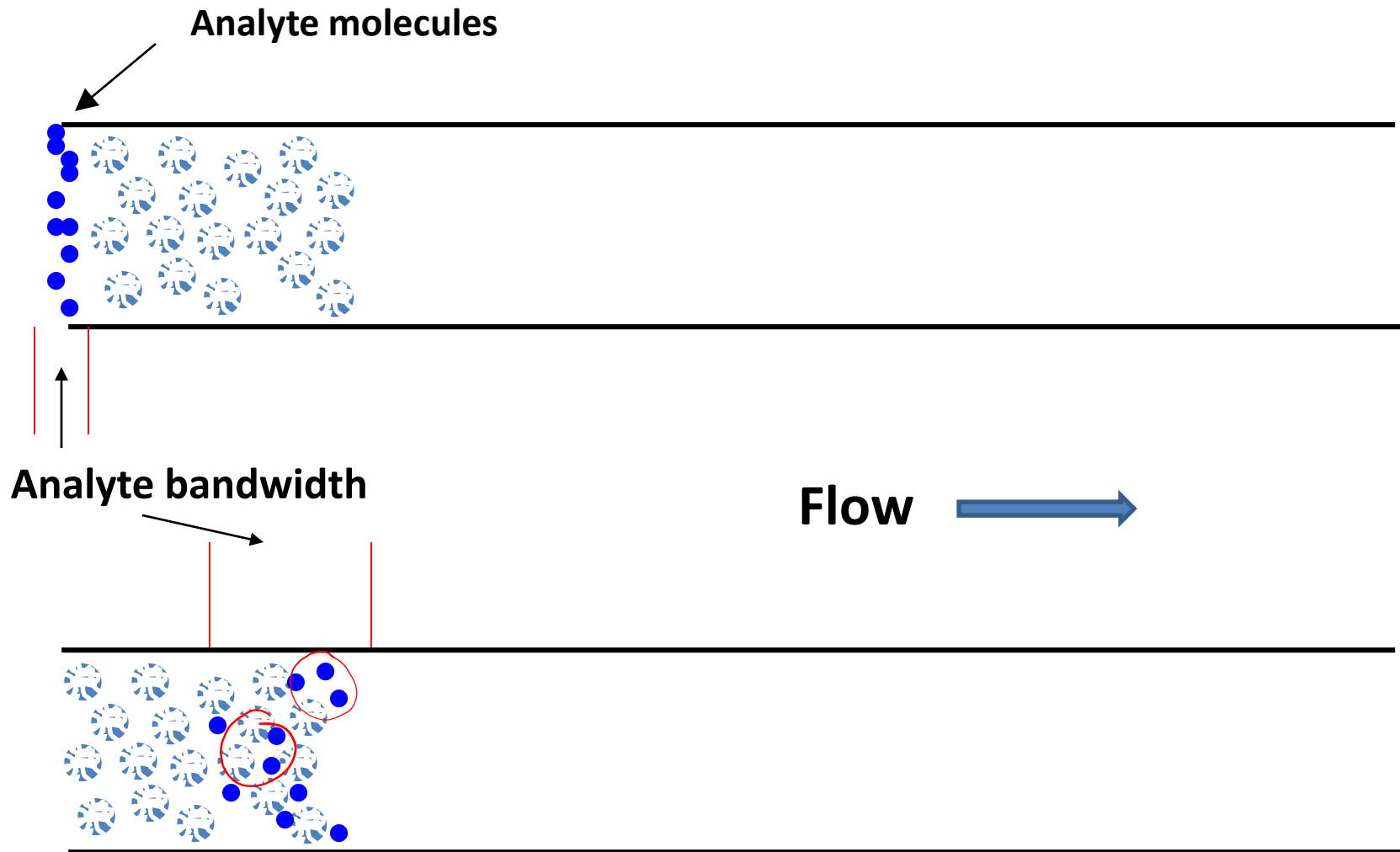
Suppose you have are running an open tubular GC column using helium as the mobile phase, and you switch to nitrogen because you've run out of helium. Draw two van Deemter curves for these two situations on one graph. Now, assume you are working at a mobile phase velocity that is $2 \cdot u_{m,opt}$ for the helium curve. Draw a chromatogram that shows two peaks separated in the helium case with a resolution of 1.5. Now, on the same graph, draw a chromatogram for the nitrogen case. For each of these, be as quantitative as you can with the information provided.

Part III – Peak Broadening in Liquid Chromatography

For Open Tubular Columns

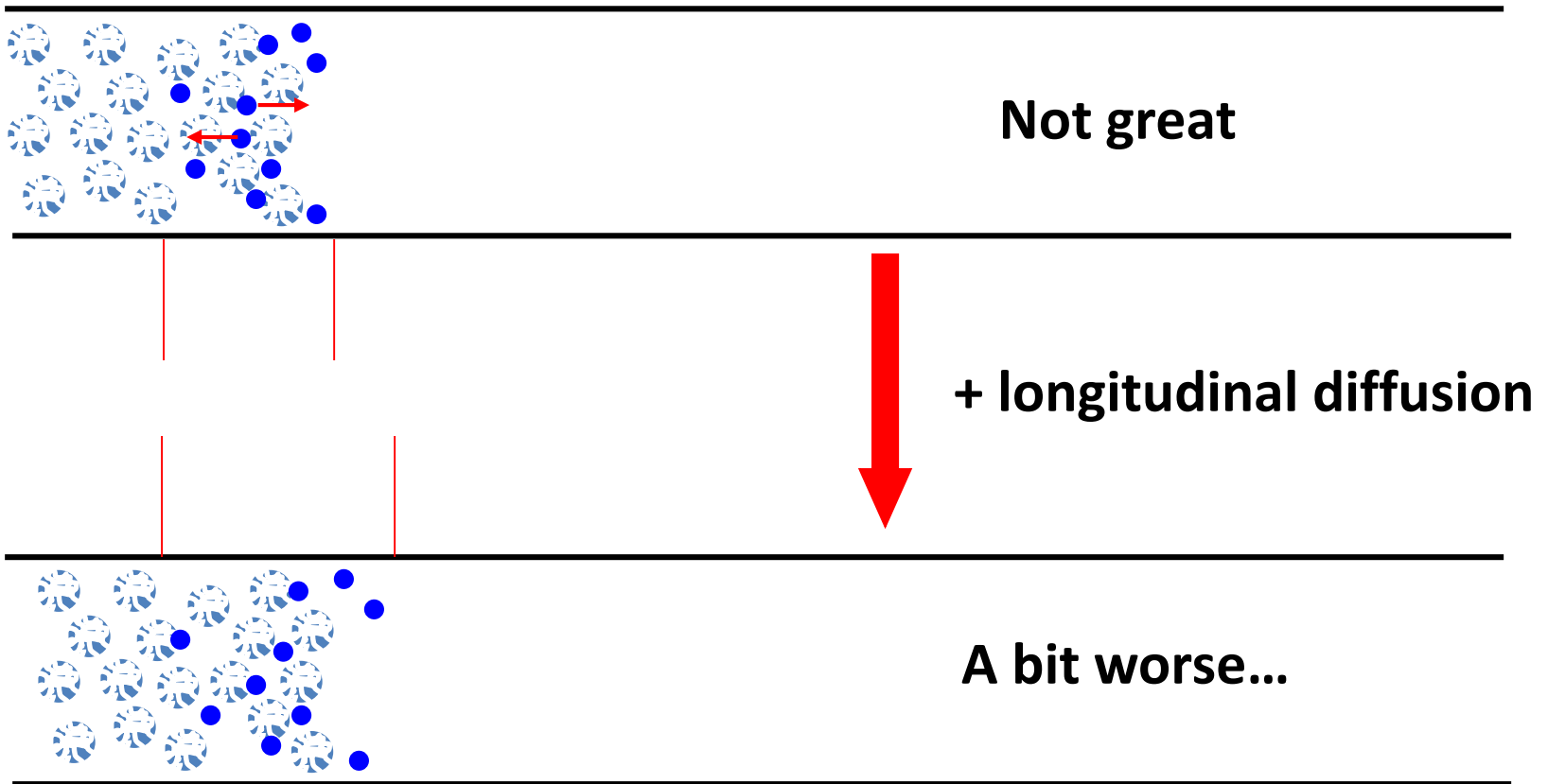
| | To Make H Small... | Practical Consequence/Problem |
|-------------|--------------------|-------------------------------|
| H_{axial} | | |
| $H_{l.d.}$ | | |
| $H_{s.p.}$ | | |

A-term Broadening in a Packed Bed – the ‘Multi-Path’ Term



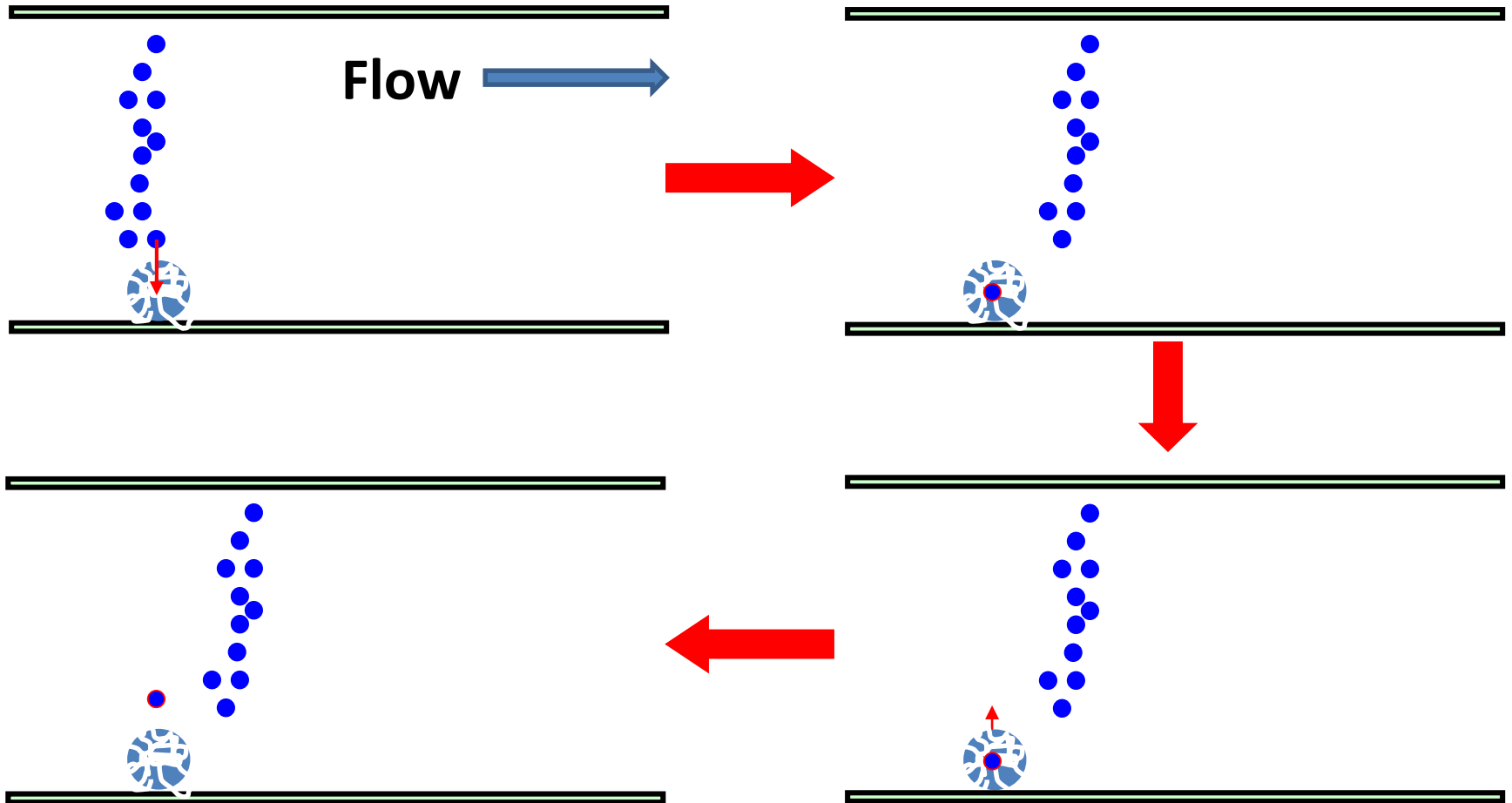
$$H_A \propto d_p$$

Longitudinal diffusion is another problem...



$$H_B \propto \frac{D_m}{u_e}$$

And finally...slow diffusion out of the stationary zone...



$$H_C \propto \frac{u_e d_p^2}{D_m}$$

How to Make H Small??

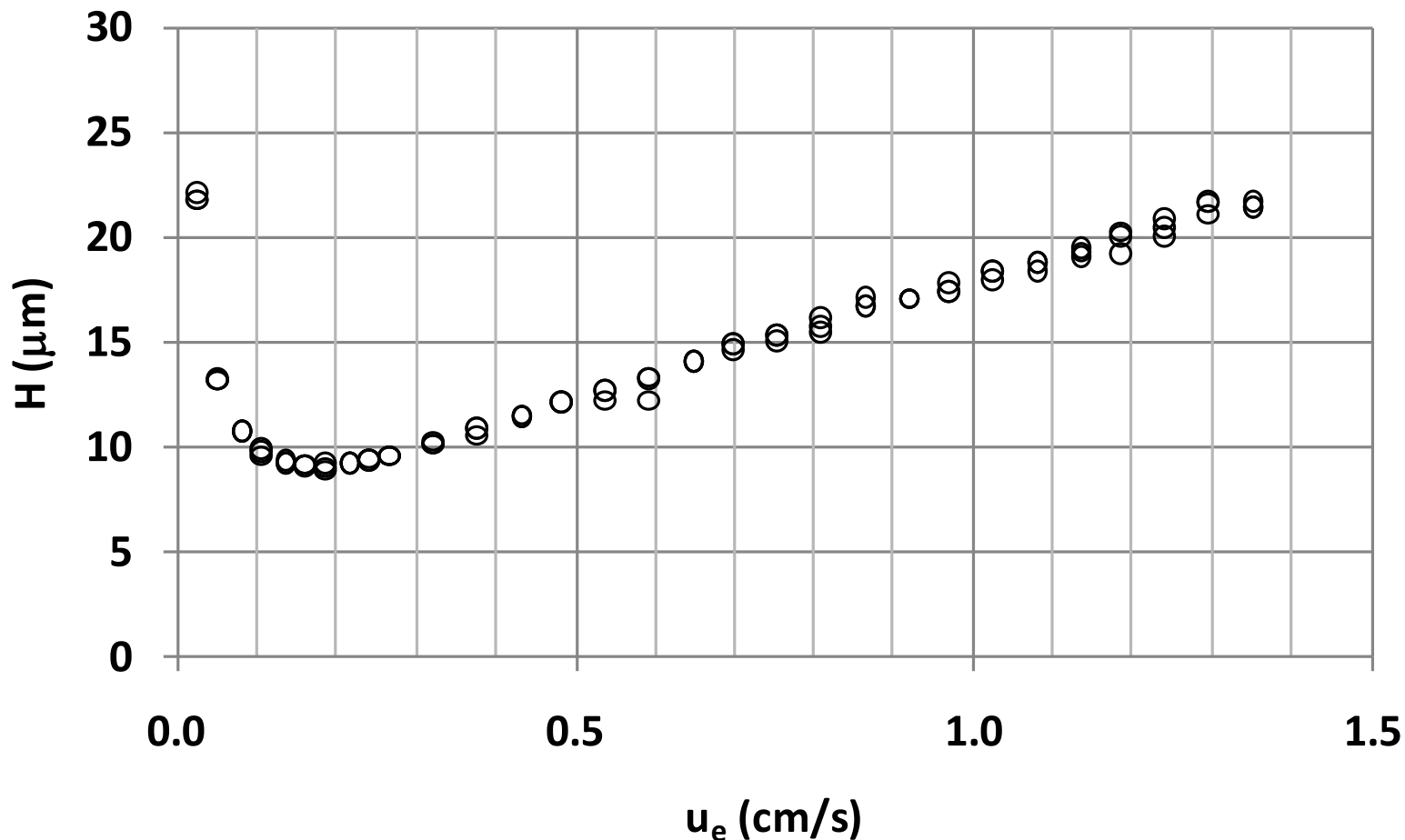
| | To Make H Small... | Practical Consequence/Problem |
|-------|--------------------|-------------------------------|
| H_A | | |
| | | |
| | | |
| H_B | | |
| | | |
| H_C | | |
| | | |
| | | |
| | | |

An important fundamental observation: Peaks that are more retained by a column come out of the column with a larger peak width.

An important fundamental question: What is the physical basis for this?

2.

1. Suppose you have a RPLC column packed with 5 μm particles. You make the measurements needed to construct the van Deemter curve shown below. How will the curve change if you do the same experiment with a column packed with 2.5 μm particles?



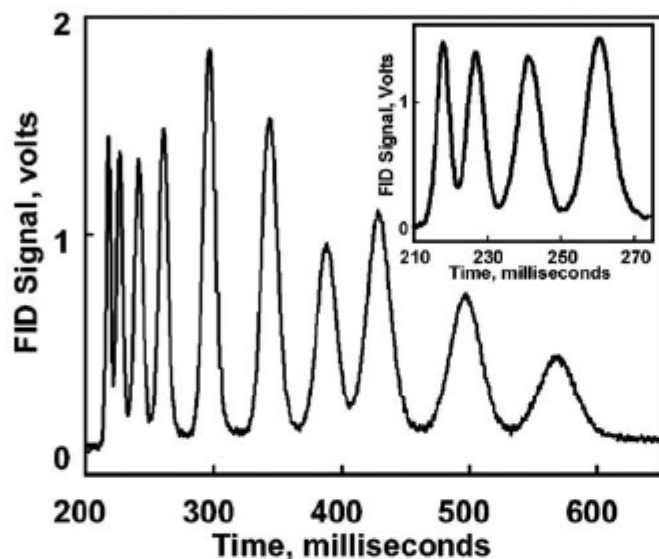
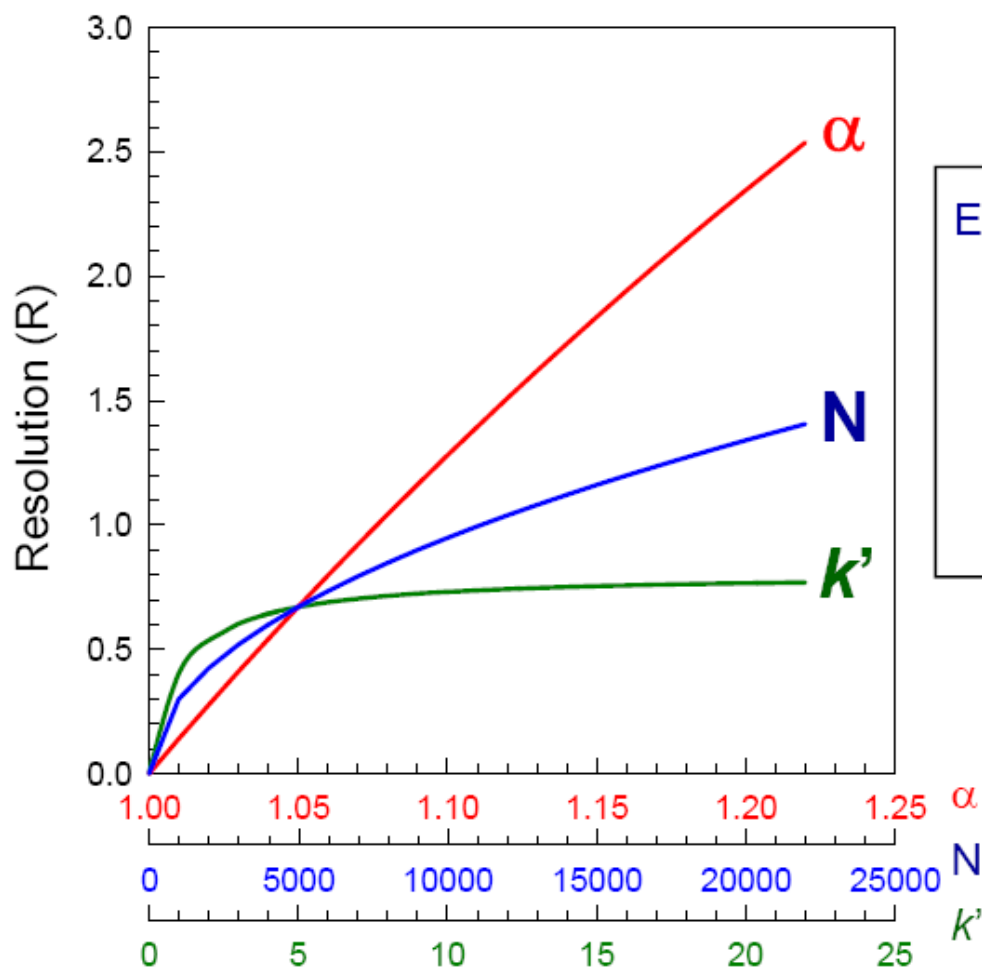


Figure 8. A 10-component separation using a 2-m column with a column absolute head pressure of 145 psi (~ 943 cm/s average linear flow velocity, ~ 21 mL/min volumetric flow rate at the column outlet). All other parameters utilized for the 1-m experiment outlined in Figure 3A (inlet pressure, oven temperature, initial injection volume, valve 2 delay time of 2.5 ms, etc.) held constant. Retention order: methanol, acetone, hexane, benzene, toluene, chlorobenzene, anisole, propylbenzene, isobutylbenzene, and butylbenzene.

Part IV – Optimization of Separations

| Column Type | Open Tube | | Open Tube | | Open Tube/Packed Bed | |
|-----------------------|-----------------------------------------|-----|-----------------------------|-----|--------------------------------------|-----|
| Column Diameter | Narrow ~ 0.1-0.3 mm | | Narrow ~ 0.25-0.32 mm | | Wide > 0.5 mm | |
| S.P. Film Thickness | Thin ~ 0.2 microns | | Thick ~ 1-2 microns | | Thick - 2-5 microns (open tube only) | |
| | | Why | | Why | | Why |
| Efficiency | Best | | Good | | Poor | |
| Separation speed | Fast | | Moderate | | Slow | |
| Analyte Capacity | Poor | | Good | | Best | |
| | | | | | | |
| Preferred Application | High speed, high resolution separations | | Low boiling point compounds | | Anybody can do it | |
| | High boiling point compounds | | Trace analysis | | Low boiling point compounds | |
| | Thermally unstable compounds | | | | | |

Contributions to Resolution



| Efficiency | Selectivity | Retention |
|----------------------|---------------------------|-------------------|
| ↓ | ↓ | ↓ |
| $\frac{\sqrt{N}}{4}$ | $\frac{\alpha-1}{\alpha}$ | $\frac{k'}{k'+1}$ |

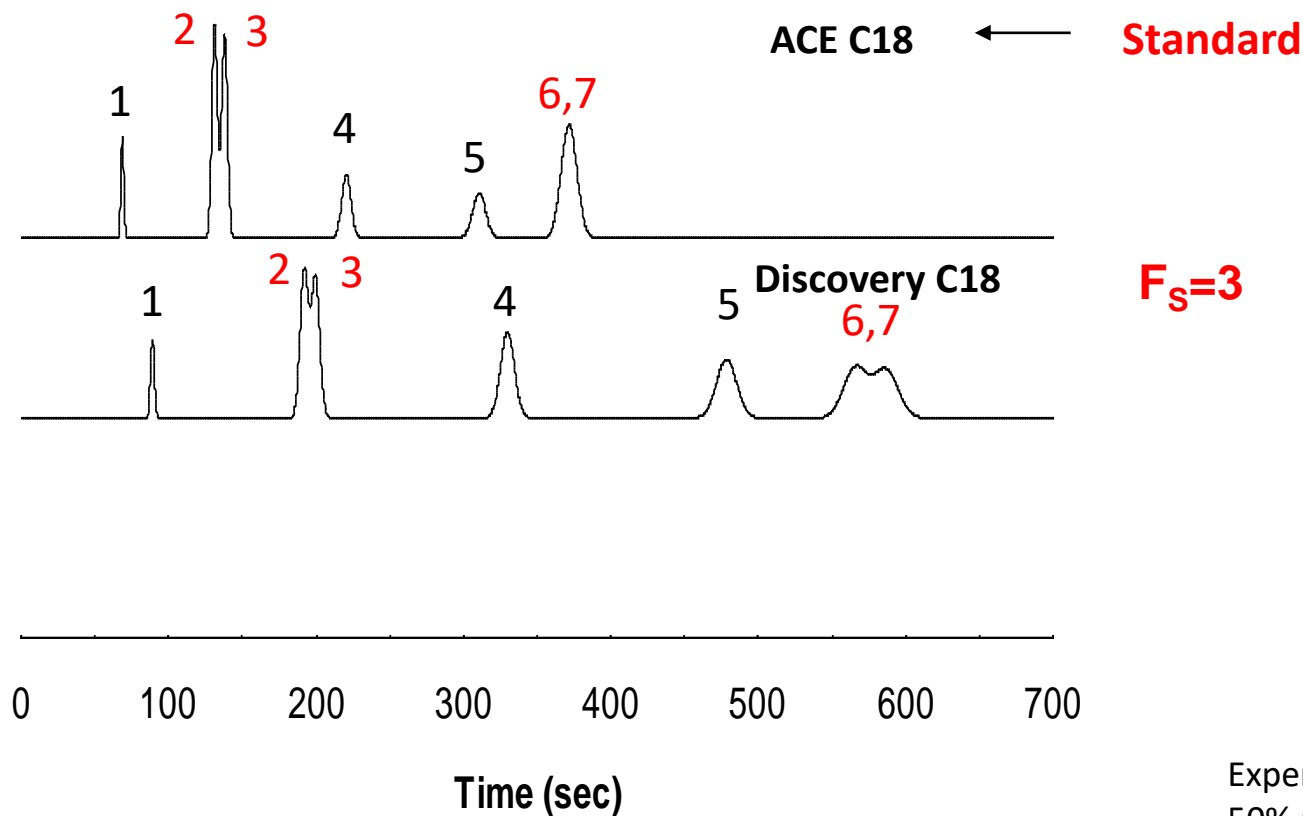
$$R = \frac{\sqrt{N}}{4} \cdot \frac{\alpha-1}{\alpha} \cdot \frac{k'}{k'+1}$$

❖ **Small changes in selectivity (α) have the greatest impact on resolution.**

The Beauty of Snyder's Model

- Quantitative comparison of selectivity for two columns by a single parameter:

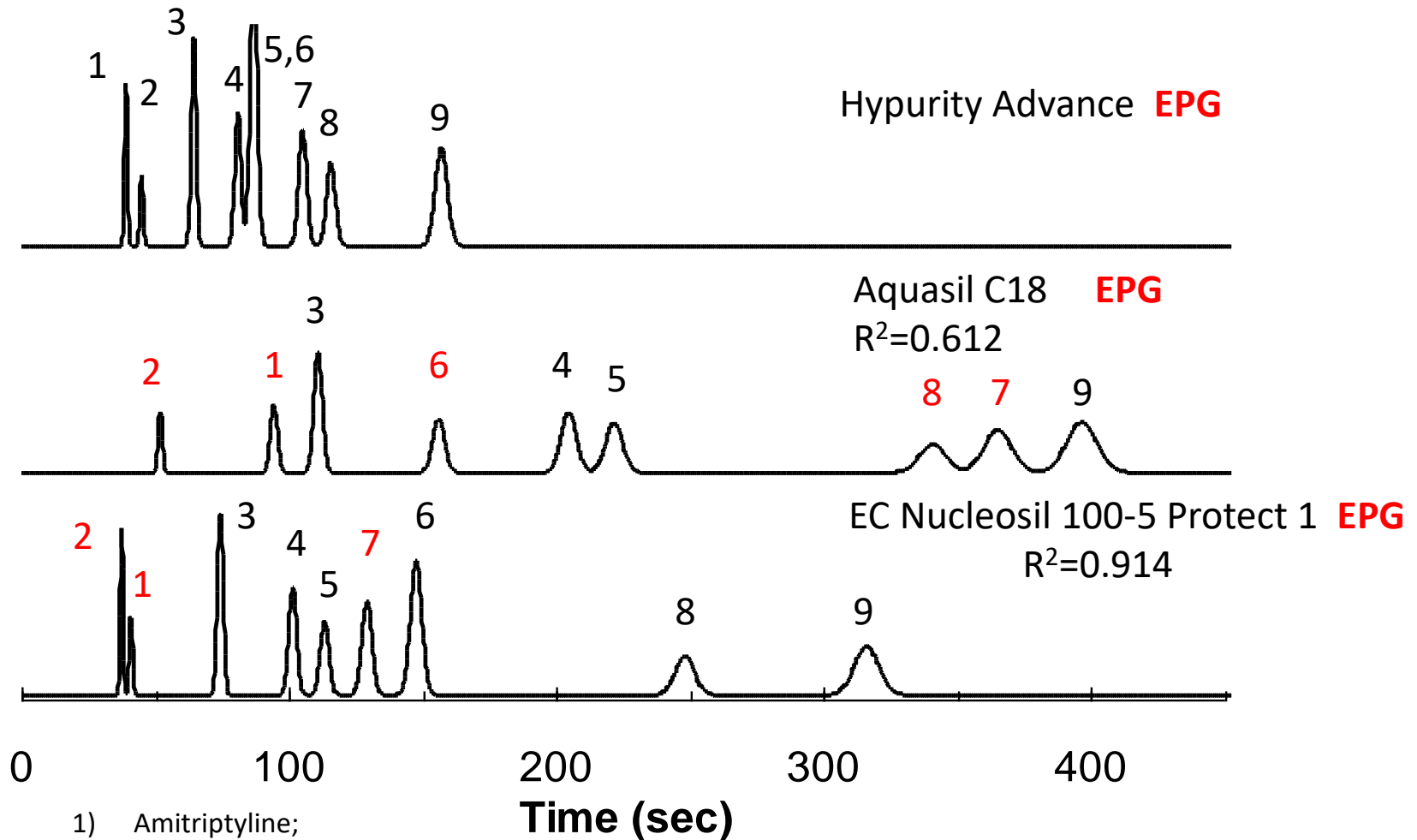
$$F_s = \{12.5(H_2 - H_1)^2 + 100(S_2 - S_1)^2 + 30(A_2 - A_1)^2 + 143(B_2 - B_1)^2 + 83(C_2 - C_1)^2\}^{1/2}$$



- (1) 4-nitrophenol;
- (2) 5-phenylpentanol;
- (3) anisole;
- (4) toluene;
- (5) cis-chalcone;
- (6) trans-chalcone;
- (7) mefenamic acid.

Experimental conditions:
50% acetonitrile/pH 2.8 buffer;
35 °C; 1.0 ml/min

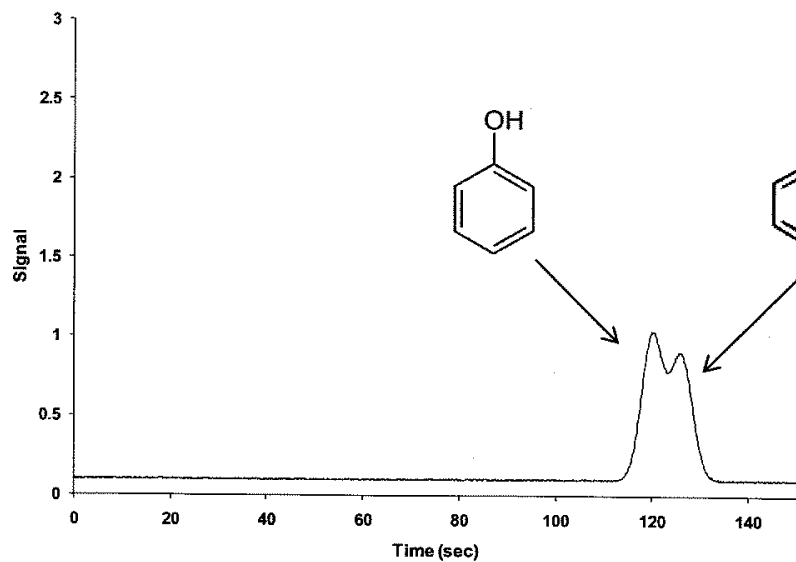
Selectivity Comparison of Three EPG Phases



- 1) Amitriptyline;
- 2) N,N-dimethylacetamide;
- 3) Acetophenone;
- 4) Toluene;
- 5) 5-phenylpentanol;

- 6) Trans-chalcone;
- 7) 4-n-butylbenzoic acid;
- 8) Cis-chalcone;
- 9) Mefenamic acid

Experimental conditions:
 50% acetonitrile/pH 2.8 buffer;
 35 °C; 1.0 ml/min



Assume $t_m = 25$ sec. in all cases, and
the m.p. velocity = $2 \cdot u_{e,opt}$

